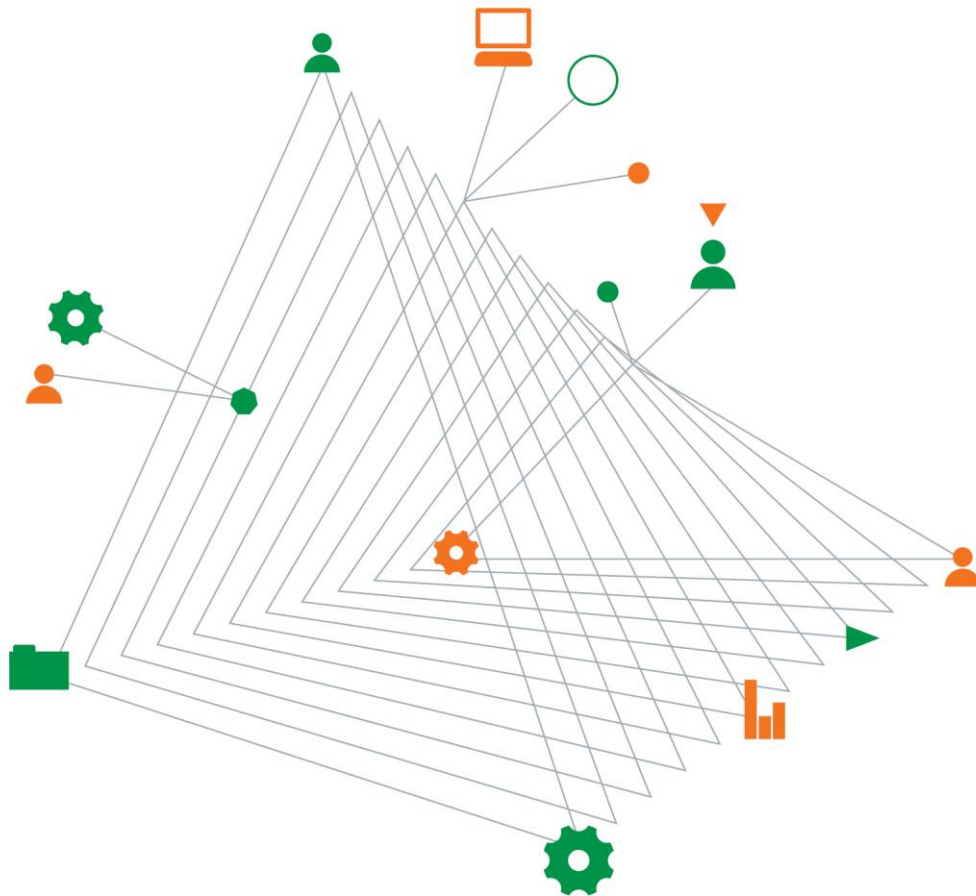


Hugh Green Limited

Geotechnical Completion Report  
on Donegal Stud Stage 8 at 64 Thomas Road,  
Flat Bush, Auckland

Project No GENZAUCK16403AC

6 December 2016



Experience  
comes to life  
when it is  
powered by  
expertise

Donegal Stud Stage 8 at 64 Thomas Road,  
Flat Bush, Auckland

Hugh Green Limited  
Donegal Stud  
C/- Harrison Grierson Consultants Limited  
PO Box 5760  
Wellesley Street  
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Prepared by  
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Our Reference: GENZAUCK16403AC

6 December 2016

Dear Will

**RE: Geotechnical Completion Report for Residential Subdivision at Donegal Stud Stage 8,  
64 Thomas Road, Flat Bush, Auckland**

This report presents all supporting geotechnical data and our Suitability Statement in relation to land development works undertaken at the above location.

It has been prepared in accordance with instructions received from Harrison Grierson Consultants Limited and forms part of the documentation required by Auckland Council to achieve certification under Section 224(c) of the Resource Management Act.

If you have any queries or you require any further clarification on any aspects of this report, please do not hesitate to contact the undersigned.

For and on behalf of Coffey



**Kah-Weng Ho**  
Senior Principal

## Quality information

### Revision history

Revision	Description	Date	Author	Reviewer	Signatory
0	Final	06/12/2016	RB	PM	RB

### Distribution

Report Status	No. of copies	Format	Distributed to	Date
Final	1	PDF	Hugh Green Limited	06/12/2016
Final	1	PDF	Auckland Council	06/12/2016
Final	1	Original	Coffey Geotechnics (NZ) Limited	06/12/2016

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# 1. Introduction and Description of Subdivision

This Geotechnical Completion Report (GCR) has been prepared for Hugh Green Limited as part of the documentation required to be submitted to the Auckland Council following residential subdivisional development.

It contains our Suitability Statement, relevant test data and the Harrison Grierson Consultants Limited as-built plan set relating to Stage 8 of the Donegal Stud Residential Subdivision as follows:

Table 1: Harrison Grierson Consultants Limited As-Built Plans

Title	Reference No.	Date
Stage 8 Finished Contours As-Built	136822-AB200	28 November 2016
Stage 8 Cut Fill As-Built	136822-AB220	28 November 2016
Stage 8 Pavement As-Built	136822-AB301	30 November 2016
Stage 8 Pavement As-Built Sections Sheet 1 of 4	136822-AB330	30 November 2016
Stage 8 Pavement As-Built Sections Sheet 2 of 4	136822-AB331	30 November 2016
Stage 8 Pavement As-Built Sections Sheet 3 of 4	136822-AB332	30 November 2016
Stage 8 Pavement As-Built Sections Sheet 4 of 4	136822-AB333	30 November 2016

This report covers the construction period early-August 2016 to mid-November 2016. It is intended to be used for certification purposes for:

- 73 residential lots numbered 1 to 73; and
- 8 new roads named Road 1 to Road 8.

Stage 8 of the subdivision is located at 64 Thomas Road and as can be seen on the cut fill as-built plan, most of the lots have been partly or totally affected by filling, to a maximum depth of up to approximately 1.5 metres.

Pre-existing underfill drains and filling are located within the north western portion of the site, refer Harrison Grierson Consultants limited Finished Contours As-Built Plan presented in Appendix 1. The underfill drains and associated filling are expressly excluded from this certification.

## 2. Related Reports

Geotechnical Reports prepared on the subject land by this consultancy are as follows:

- Geotechnical Investigation Report on Donegal Stud subdivision, reference GENZNEWP15126; dated 26 May 2011;
- Earthworks Plan Review on Donegal stud Stage 2 to 4, reference GENZAUCK15126AC, dated 22 August 2012;
- Earthworks Plan Review on Donegal stud Stage 6, reference GENZAUCK15126AF, dated 21 August 2013;
- Geotechnical Completion Report on Donegal Stud Stage 4, reference GENZAUCK15126AC, dated 11 November 2013;

- Geotechnical Completion Report on Donegal Stud Stage 6, reference GENZAUCK15126AF, dated 16 June 2014;
- Geotechnical Investigation Report on 62 Thomas Road, Flat Bush, reference GENZNEWP16403, dated 18 December 2014; and
- Plan Review for Proposed Earthworks (our reference GENZAUCK16403AC dated 22 July 2015 supporting the subdivisional development of Donegal Stud, Stage 8.

The conclusions and recommendations of those documents (where relevant) have been reviewed during the preparation of this report.

## **3. Earthworks Operations**

### **3.1. Plant**

The main items of plant used by the Contractor, Ross Reid Contractors Limited were:

- 2 x Motor scrapers;
- 1 x Bulldozer;
- 2x Moxy Dump Truck;
- 4 x Excavators;
- 1 x Tractor;
- 1 x Water Cart;
- 2 x 825 Caterpillar Sheep Foot compactors;
- 1 x Grader; and
- 2 x Vibrating Drum Roller.

### **3.2. Construction Programme**

Earthworks were conducted within the area defined as Donegal Stud Stage 8 during the previous development of Donegal Park Stages 1A to 1C in the construction season of 1997 to 1998. During this time a series of underfill drains were placed within a gully network prior to engineered fill being placed. The extent and location of the underfill drains is shown on the Harrison Grierson, Stage 8 Finished Contours As-Built Plan, refer Appendix 1. Further, the original Harrison Grierson Depth of Fill Plan, fill compaction test records and Statement of Professional Opinion as to Suitability of Land for Residential Development are contained in Appendix D. These works do not form part of this certification.

Earthworks operations for Stage 8 commenced in mid-December 2015 with the construction of a temporary silt pond in the north western corner of the development area. Prior to the commencement of the enabling works a horse stable was demolished and removed from site and during this process, uncertified filling was uncovered beneath the stables. At this time a trial pit investigation was conducted to ascertain the extent and quality of the uncertified fill materials. Due to the high content of debris contained within the uncertified fill material, it was decided that the material was to be uplifted and stockpiled beyond the northern boundary of the Stage 8 development area.

The formation of the temporary silt pond was completed by mid-January 2016 and at this time topsoil stripping commenced. By late February 2016 the bulk of the uncertified filling and topsoil had been

removed from site. Prior to the commencement of bulk filling an area of soft ground noted during the process of topsoil stripping was undercut by 500mm. The undercut materials were then mixed and conditioned then placed back into the undercut as engineer certified filling.

Bulk earthworks continued steadily with the majority of the cut / fill being completed by April 2016. Prior to the completion of the bulk earthworks (late March 2016) a small fill area located on the north eastern boundary (adjacent to a gully system) was prepared to receive fill. Fill was placed at this location to form a batter / abutment for a road culvert crossing that is to be formed at a later date (during the development the greater 64 Thomas Road development area). Due to the toe of the batter being located within the gully and on soft alluvial sediments, it was decided that a 0.5m undercut should be performed to remove the unsuitable alluvial deposits. The unsuitable deposits were then replaced by compacted Soft Pit Run (SPR) hardfill prior to the batter being formed with cohesive fill.

By mid-May earthworks primarily focussed on the resspreading of topsoil, the installation of site services and the construction of the internal roads. Due to the prevailing inclement weather conditions it was decided to stabilise the road subgrades with a mixture of lime and cement so that earthworks, including road construction could continue over the winter period. However, due to elevated soil moisture contents and low atmospheric temperatures, subgrade stabilisation was ineffective, particularly in the northern portion of the site.

To enable construction to continue, the roads in the northern portion of the site (Roads 1, 2, 3 and 7) were undercut by up to 600mm with the low strength subgrade materials being replaced with either black sand or compacted GAP65. By September 2016 the undercutting and replacement of the road subgrade materials in the northern portion of the site was mostly complete.

After the completion of the undercutting of the roads described above, sub-basecourse hardfill was then placed and compacted prior to kerb and channels being formed. During this period heaving of the subgrade was observed over sections of Road 4 and Road 5. The extent of the low strength subgrade was delineated and the materials were then undercut by typically 400mm with the unsuitable material being replaced by compacted GAP65.

Road subgrade preparation was completed by mid-October 2016 and at this stage the installation of the road under channel drains and formation of the road pavement commenced. During the bulk earthworks (cut) phase in this area and during the installation of the under channel drains (for Road 2 and Road 5) the pre-existing underfill drain located in and beyond Lot 36 was intercepted or exposed at the surface of the subgrade. As a result, this drain coil was removed in its entirety.

Construction of the road basecourse and installation of site services continues steadily until their completion in late November 2016.

## **4. Quality Assurance and Controls**

### **4.1. Inspections**

During the earthworks engineering inspections were undertaken on a regular basis to assess compliance with NZS 4431 and our project specific recommendations and specifications. Project specific inspections were required on this stage of the development for:

- Topsoil stripping;
- Observed bulk cut to fill operations; and
- Observe the removal of unsuitable fill.



## 4.2. Quality Control Criteria

### 4.2.1. Compaction

Due to the varying soil types being used as filling, the compaction control criteria of minimum allowable shear strength and maximum allowable air voids were mainly used for quality assurance purposes.

Specification details were as follows:

#### Minimum Shear Strength and Maximum Air Voids Method

Table 2: Minimum Shear Strength and Maximum Air Voids Method

(a)	<u>Air Voids Percentage</u>	
	(As defined in NZS 4402)	
	General Fill	
	Average value less than	10%
	Maximum single value	12%
	Maximum value	
(b)	<u>Undrained Shear Strength</u>	
	(Measured by Pilcon shear vane - calibrated using NZGS 2001 method)	
	General fill	
	Average value not less than	140 kPa
	Minimum single value	120 kPa

## 4.3. Quality Assurance Testing

### 4.3.1. Compaction

Regular insitu density, strength and water content tests were carried out on all areas of the filling at or in excess of the frequency recommended by NZS 4431. Within Stage 8 there was one occasion where the filling failed to meet the aforementioned criteria. The test failure was relayed to the site foreman and/or his staff, and to the best of our knowledge the affected area of fill was re-worked as necessary. Further testing was carried out until compliance with the standards was achieved.

## 5. Project Evaluation

### 5.1. Bearing Capacity and Settlement of Building Foundations

Following the completion of earthworks operations, we returned to the site on 11 August 2016 and 17 November 2016 and drilled a series of hand auger boreholes at appropriate natural ground locations in order to evaluate likely foundation options for future building development. Topsoil depths on each lot were also assessed at this time.

At current subgrade levels all filled and undisturbed natural ground has a geotechnical ultimate bearing capacity of 300 kPa within the influence of conventional shallow residential building foundation loads.

It should be noted that NZS 3604 only allows a maximum backfill depth of 600mm over the building platform of a dwelling unless an Engineering design solution is proposed, on account of the risk of induced consolidation of the subsoils caused by the weight of the backfill.

## **5.2. Expansive Soils**

Two sets of Expansive soil tests were carried out on samples selected from within the zone of likely influence of shallow building foundations in Stage 8 development area.

These tests were carried out in accordance with NZS 4402, "Methods of Testing Soils for Civil Engineering Purposes" test section 2 and were primarily intended to assess the Expansive Classes of the site materials as defined in AS 2870, "Residential Slabs and Footings – Construction".

All test results are IANZ (International Accreditation New Zealand) endorsed and full details are appended.

The AS 2870 Site Class for this subdivision is M (moderate), and is based on the laboratory results together with our visual-tactile assessment and local knowledge. Specific design alternatives for this Site Class are presented in the Suitability Statement.

## **5.3. Fill Induced Settlement**

As a result of our pre-fill inspections and quality control testing, we are of the opinion that induced differential settlements beneath or within the certified filling due to its imposed weight should be insignificant with respect to conventional NZS 3604 residential building developments.

## **5.4. Vegetation Cover**

Wherever practical on sloping land beyond building platform areas all existing grass cover should be maintained and even supplemented with new plantings. Any vegetation cleared beyond the immediate area of building platforms for temporary construction purposes should be replanted replaced as soon as possible.

The contribution of appropriate vegetation cover to overall sediment and erosion control should not be underestimated.

## **5.5. Stormwater Controls**

It is important on all sloping lots that due care is paid to the design and construction of appropriate stormwater disposal systems. These systems should serve to collect all runoff from roofs, decks and paved areas, together with discharges from retaining wall drains and other subsoil drains and should connect directly into the public stormwater drainage network.

## **5.6. Service Trenches**

As is normal on all subdivisions, building developments involving foundations within a 45 degree zone of influence from pipe inverts will require engineering input. However, it is unlikely to be an issue for Stage 8 based on the as-built plans.

## **5.7. Road Subgrades**

Dynamic Cone Penetrometer (DCP) testing was undertaken at regular intervals on the road subgrades and the results were subsequently forwarded to Harrison Grierson Consultants Limited for pavement design purposes. We understand that all roads within Stage 8 were either stabilised with lime and cement or undercut and replaced with black sand and /or GAP65 hardfill, as depicted on Harrison Grierson Consultants limited Stage 8 Pavement As-Built plan, reference 136822-AB301, dated 30 November 2016, refer Appendix 1.

## **5.8. Underfill Drains**

During the development of Donegal Park Stages 1A to 1C a series of perforated underfill drains were placed in the mucked out gully inverts to tap groundwater seepages prior to filling, as required by NZS 4431.

These drains were intended to intercept localised groundwater seepages and springs during earthworks and to help provide general control over groundwater levels. They are buried beneath 0.5 to 1.5m depth of engineered filling placed during the construction season of 1997 to 1998. In the event of any foundation solutions being constructed in the 45 degree zone of influence of these drains, they must be endorsed by an Engineer to ensure they do not compromise the function of the drains.

These drains are not covered under this certification.

## **5.9. Topsoil**

Topsoil depths in likely building platform areas were checked by the drilling of a borehole in the approximate centre of each of the lots. Our findings, which are indicative only and subject to variation at other locations, show that likely topsoil depths are between 50 mm and 300 mm.

## **5.10. Contractor's Work**

We have relied on the Contractor's work practices and assume that the works have been carried out in accordance with:

- (i) The approved Contract drawings and design details,
- (ii) The approved Contract specifications,
- (iii) Authorised Variations to (i) and (ii) during the execution of the works,
- (iv) The conditions of Resource, Earthworks and Building Consents where applicable,
- (v) The relevant Coffey Geotechnics reports, recommendations and site instructions,

and that all as-built information and other details provided to the Client and/or Coffey Geotechnics are accurate and correct in all respects.

## 6. Statement of Professional Opinion as to the Suitability of Land for Building Development

I, Kah-Weng Ho, of Coffey Geotechnics (NZ) Limited, Auckland, hereby confirm that:

1. I am a Chartered Professional Engineer experienced in the field of geotechnical engineering as defined in section 1.2.3 of NZS 4404 and was retained by the Developer as the Geotechnical Engineer on Stage 8 of the Donegal Stud residential subdivision, Flat Bush.
2. The extent of preliminary investigations carried out to date are described in Geotechnical Investigation Report, reference GENZAUCK16403AC, dated 18 December 2014. The conclusions and recommendations of that document have been re-evaluated in the preparation of this report. Details of the results of all tests carried out are appended.
3. In my professional opinion, not to be construed as a guarantee, I consider that:
  - a. The earth fills shown on the appended Harrison Grierson Consultants Limited Cut-Fill As-Built Plan have been placed in compliance with NZS 4431 and related documents.
  - b. The function of all underfill drains on Lots 36, 72 and 73 must not be impaired by any building development or landscaping works. In particular, any bored or driven piles must be positioned to avoid damaging these drains. The presence of all such drains should be recorded on Council's hazard register.
  - c. A geotechnical ultimate bearing capacity of 300 kPa may be assumed for shallow foundation design on all lots.

Where a geotechnical bearing capacity greater than 300 kPa is required, (i.e. outside the limits of NZS 3604, such as when piling is undertaken), further specific site investigation and design of foundations should be carried out prior to building consent application.

- d. The backfilling and compaction of the stormwater and sanitary sewer trenches on this subdivision has where possible been carried out to appropriate standards having regard for the prevailing ground conditions and associated compaction induced pipe loadings.

Nevertheless, no building development should take place within the 45 degree zone of influence of drain inverts unless endorsed by specific site investigations, foundation designs and by construction inspections undertaken by a Chartered Professional Engineer experienced in geomechanics to ensure that lateral stability and differential settlement issues are addressed and that building loads are transferred beyond the influence of the pipe and the trench backfill.

- e. The assessed AS 2870:2011 expansive site Class for all lots is M (moderate).
    - f. Subject to the geotechnical recommendations and expansive soil assessment associated with 3(b), 3(c) 3(d) and 3(e) above:
      - (i) The cut, filled and original ground within residential lot boundaries is generally suitable for residential buildings constructed in accordance with NZS 3604 (that incorporates specific foundation and associated structural design on account of the expansive soils site class) and related documents.
      - (ii) On all lots foundation design may be carried out in accordance with AS 2870:2011 (Class M) or alternatively, a specific foundation and structural design may be undertaken by a Chartered Professional Engineer who should allow for expansive soil effects in the design. The minimum recommended foundation depth below cleared ground level following topsoil removal and benching of building platform areas is 600mm for NZS3604 type strip and pad foundations.
4. Road subgrades have been formed having due regard for slope stability and settlement, although CBR values will likely vary between natural and filled ground as is to be expected.

## 7. Limitations

The as-built plans and the professional opinion contained within this report are furnished to the Auckland Council and Hugh Green Limited for their purposes alone on the express condition that they will not be relied upon by any other person. Prospective purchasers should still satisfy themselves as to any specific conditions pertaining to their particular land interest.

The appended table summarises the status of each residential lot covered by this Suitability Statement.

For and on behalf of Coffey

Prepared By:



**Ray Berry**  
Senior Engineering Geologist

Authorised By:



**Kah-Weng Ho**  
Senior Principal

Table 6: Suitability Statement Summary

Lot No.	Comments	Topsoil Depth (mm)	Ultimate Bearing (kPa)	AS2870:2011 Class
1	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	300	300	M
2	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
3	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	100	300	M
4	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
5	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	150	300	M
6	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
7	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	75	300	M
8	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	250	300	M
9	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	150	300	M
10	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	250	300	M
11	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	100	300	M
12	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	150	300	M
13	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	100	300	M
14	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	100	300	M
15	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	150	300	M
16	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
17	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	250	300	M
18	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	250	300	M
19	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
20	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	175	300	M
21	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	50	300	M
22	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	100	300	M
23	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M

Lot No.	Comments	Topsoil Depth (mm)	Ultimate Bearing (kPa)	AS2870:2011 Class
24	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	175	300	M
25	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	100	300	M
26	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	150	300	M
27	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
28	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	250	300	M
29	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
30	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
31	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	250	300	M
32	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
33	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	225	300	M
34	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	75	300	M
35	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
36	Buried underfill drain to be preserved (refer section 6.3(b)). AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	175	300	M
37	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	50	300	M
38	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	75	300	M
39	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
40	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	175	300	M
41	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
42	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	250	300	M
43	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	300	300	M
44	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	300	300	M
45	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	250	300	M
46	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	300	300	M

Lot No.	Comments	Topsoil Depth (mm)	Ultimate Bearing (kPa)	AS2870:2011 Class
47	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	125	300	M
48	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	175	300	M
49	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	150	300	M
50	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	75	300	M
51	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
52	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
53	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	225	300	M
54	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	225	300	M
55	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	175	300	M
56	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
57	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
58	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	100	300	M
59	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
60	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	150	300	M
61	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	250	300	M
62	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
63	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
64	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	300	300	M
65	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	300	300	M
66	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	250	300	M
67	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
68	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	150	300	M
69	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	150	300	M
70	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	75	300	M



Lot No.	Comments	Topsoil Depth (mm)	Ultimate Bearing (kPa)	AS2870:2011 Class
71	AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	50	300	M
72	Buried underfill drain to be preserved (refer section 6.3(b)). AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M
73	Buried underfill drain to be preserved (refer section 6.3(b)). AS 2870 foundation design or NZS 3604 with minimum footing depth 600mm.	200	300	M

**Appendix A – Harrison Grierson Consultants  
Limited As-Built Plans**





NOTES:

- ORIGIN OF LEVELS  
S 66 SO 48643  
RL 54.50m
- ORIGIN OF COORDINATES  
S 66 SO 48643  
5905356.71mN  
1770941.22mE

LEGEND

- 1.0 — FILL CONTOUR  
— -1.0 — CUT CONTOUR  
- - - - - EXTENT OF EARTHWORKS  
CUT  
FILL

ENGINEERING APPROVAL  
ENG-48683

I CERTIFY THAT THESE AS-BUILT PLANS ARE AN ACCURATE RECORD OF THE WORKS UNDERTAKEN AND THAT:

- THE COORDINATES (X,Y) ARE IN TERMS OF NZTM ON NZGD (2000), AND ARE WITHIN ±50mm.
- THE LEVELS (Z) ARE IN TERMS OF THE AUCKLAND 1946 (MSL) LINZ DATUM (DOSLI DATUM), AND ARE WITHIN ±25mm.

Signed: *WJP*  
CHARTERED PROFESSIONAL ENGINEER

Date: 28.11.16

Name: WILLIAM PLATTS

Phone: 09-917-5000

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A	AS-BUILT	WJP	28.11.16
REF	REVISIONS	BY	DATE

PROJECT: DONEGAL STUD  
THOMAS ROAD  
FLAT BUSH

TITLE: STAGE 8  
CUT FILL AS-BUILT

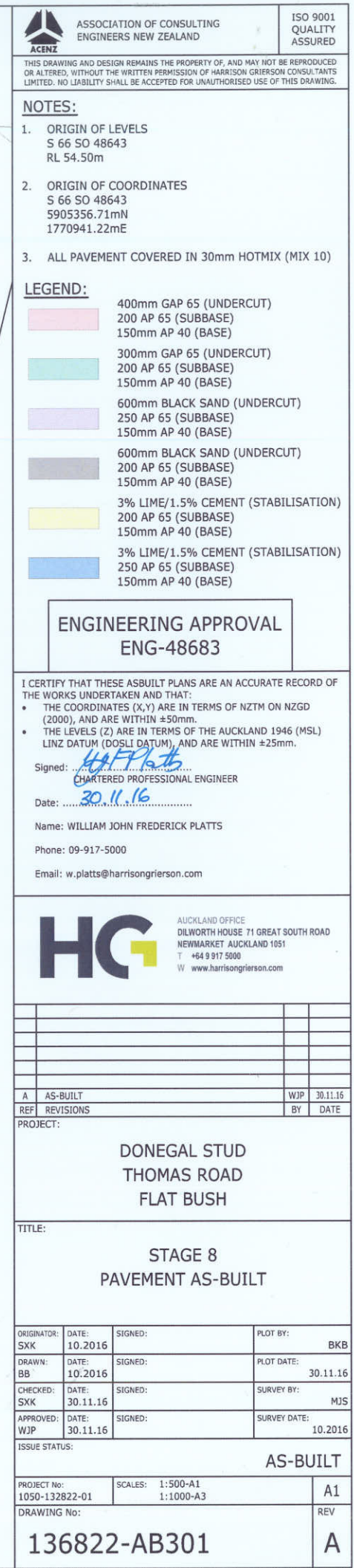
ORIGINATOR:	DATE:	SIGNED:	PLOT BY:
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CHECKED:	DATE:	SIGNED:	SURVEY BY:
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APPROVED:	DATE:	SIGNED:	SURVEY DATE:
WJP	28.11.16		10.2016

ISSUE STATUS: AS-BUILT

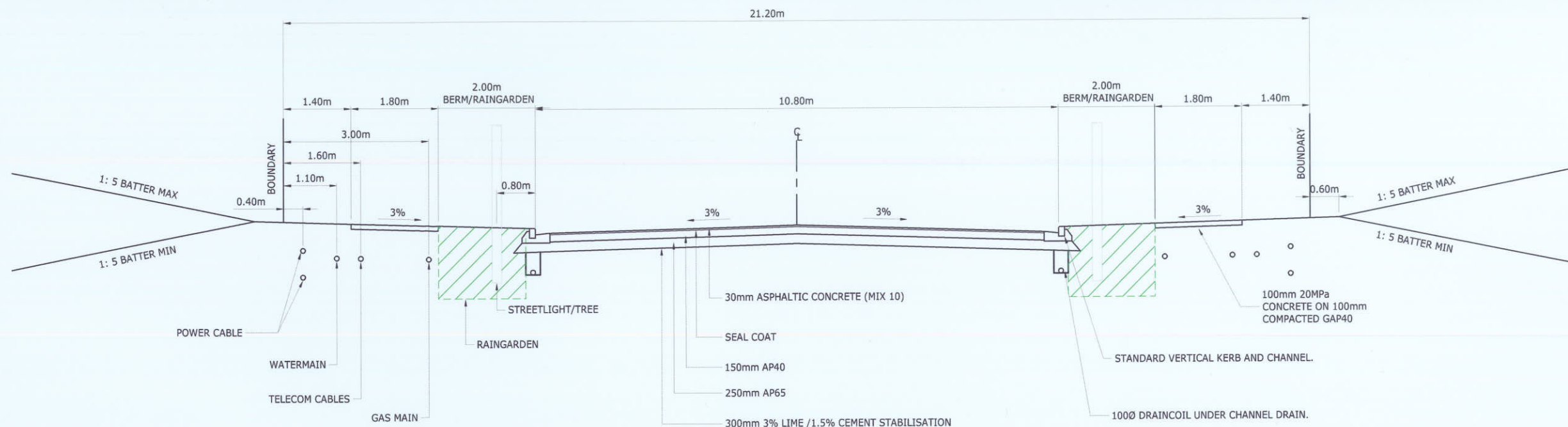
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1050-132822-01	1:1000-A3	
DRAWING No:		REV

136822-AB220 A

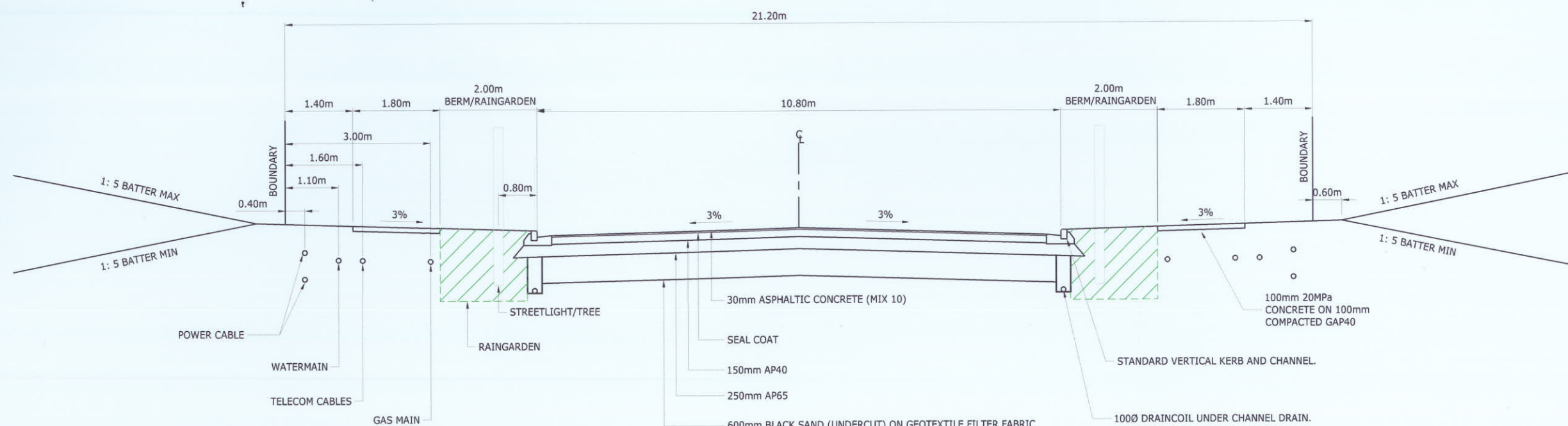








1 TYPICAL CROSS SECTION (COLLECTOR ROAD)  
AB301 SCALE 1:50 -A1 1:100 -A3 ROAD 1 (CH 5.5 - CH 189.5)



2 TYPICAL CROSS SECTION (COLLECTOR ROAD)  
AB301 SCALE 1:50 -A1 1:100 -A3 ROAD 1 (CH 189.5 - CH 231.9)

ENGINEERING APPROVAL  
ENG-48683

I CERTIFY THAT THESE ASBUILT PLANS ARE AN ACCURATE RECORD OF THE WORKS UNDERTAKEN AND THAT:

- THE COORDINATES (X,Y) ARE IN TERMS OF NZTM ON NZGD (2000), AND ARE WITHIN ±50mm.
- THE LEVELS (Z) ARE IN TERMS OF THE AUCKLAND 1946 (MSL) LINZ DATUM (DOSLI DATUM), AND ARE WITHIN ±25mm.

Signed: *WJP*  
30.11.16  
CHARTERED PROFESSIONAL ENGINEER

Date: 30.11.16

Name: WILLIAM JOHN FREDERICK PLATTS

Phone: 09-917-5000

Email: w.platts@harrissongrierson.com

**HG** AUCKLAND OFFICE  
DILWORTH HOUSE 71 GREAT SOUTH ROAD  
NEWMARKET AUCKLAND 1051  
T +64 9 917 5000  
W www.harrissongrierson.com

REF	REVISIONS	BY	DATE
A	AS-BUILT	WJP	30.11.16

PROJECT: DONEGAL STUD THOMAS ROAD FLAT BUSH

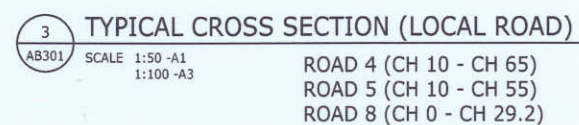
TITLE:  
STAGE 8  
PAVEMENT AS-BUILT SECTIONS  
SHEET 1 OF 4

ORIGINATOR:	DATE:	SIGNED:	PLOT BY:
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DRAWN:	DATE:	SIGNED:	PLOT DATE:
BB	11.2016		30.11.16
CHECKED:	DATE:	SIGNED:	SURVEY BY:
SXK	30.11.16		
APPROVED:	DATE:	SIGNED:	SURVEY DATE:
WJP	30.11.16		

ISSUE STATUS: AS-BUILT

PROJECT No:	SCALES:	AS SHOWN	A1
1050-132822-01			
DRAWING No:			REV

136822-AB330 A



I CERTIFY THAT THESE ASBUILT PLANS ARE AN ACCURATE RECORD OF THE WORKS UNDERTAKEN AND THAT:

- THE COORDINATES (X,Y) ARE IN TERMS OF NZTM ON NZGD (2000), AND ARE WITHIN  $\pm 50\text{mm}$ .
- THE LEVELS (Z) ARE IN TERMS OF THE AUCKLAND 1946 (MSL) LINZ DATUM (DOSLI DATUM), AND ARE WITHIN  $\pm 25\text{mm}$ .

Date: 30.11.16

Name: WILLIAM JOHN FREDERICK PLATTS

Phone: 09-917-5000

Email: [w.platts@harrisingrierson.com](mailto:w.platts@harrisingrierson.com)



REF	REVISION	DATE	BY
PROJECT:			

DONEGAL STUD  
THOMAS ROAD  
FLAT BUSH

TITLE:

STAGE 8  
PAVEMENT AS-BUILT SECTIONS  
SHEET 2 OF 4

ISSUE STATUS:

AS-BUILT

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136822-AB331

A







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## ROAD 7 (CH 10 - CH 37.8)

AB301 SCALE 1:50 -A1  
1:100 -A3



## ROAD 2 (CH 10 - CH 112.8)

AB301 SCALE 1:50 -A1  
1:100 -A1

I CERTIFY THAT THESE ASBUILT PLANS ARE AN ACCURATE RECORD OF THE WORKS UNDERTAKEN AND THAT:

- THE COORDINATES (X,Y) ARE IN TERMS OF NZTM ON NZGD (2000), AND ARE WITHIN  $\pm 50\text{mm}$ .
- THE LEVELS (Z) ARE IN TERMS OF THE AUCKLAND 1946 (MSL) LINZ DATUM (DOSLI DATUM), AND ARE WITHIN  $\pm 25\text{mm}$ .

Signed: W. F. Path  
CHARTERED PROFESSIONAL ENGINEER

Date: 30.11.16

Name: WILLIAM JOHN FREDERICK PLATTS

Phone: 09-917-5000

Email: [w.platts@harrisingrierson.com](mailto:w.platts@harrisingrierson.com)

A	AS-BUILT	WJP	30.11.
RFF	REVISIONS	BY	DATE

PROJECT:	
----------	--

DONEGAL STUD  
THOMAS ROAD  
FLAT BUSH

TITLE:	
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STAGE 8  
PAVEMENT AS-BUILT SECTIONS  
SHEET 3 OF 4

ORIGINATOR: SXX	DATE: 11.2016	SIGNED:	PLOT BY:
DRAWN: BB	DATE: 11.2016	SIGNED:	PLOT DATE: 30.11.2016
CHECKED: SXX	DATE: 30.11.16	SIGNED:	SURVEY BY:
APPROVED: WJP	DATE: 30.11.16	SIGNED:	SURVEY DATE:

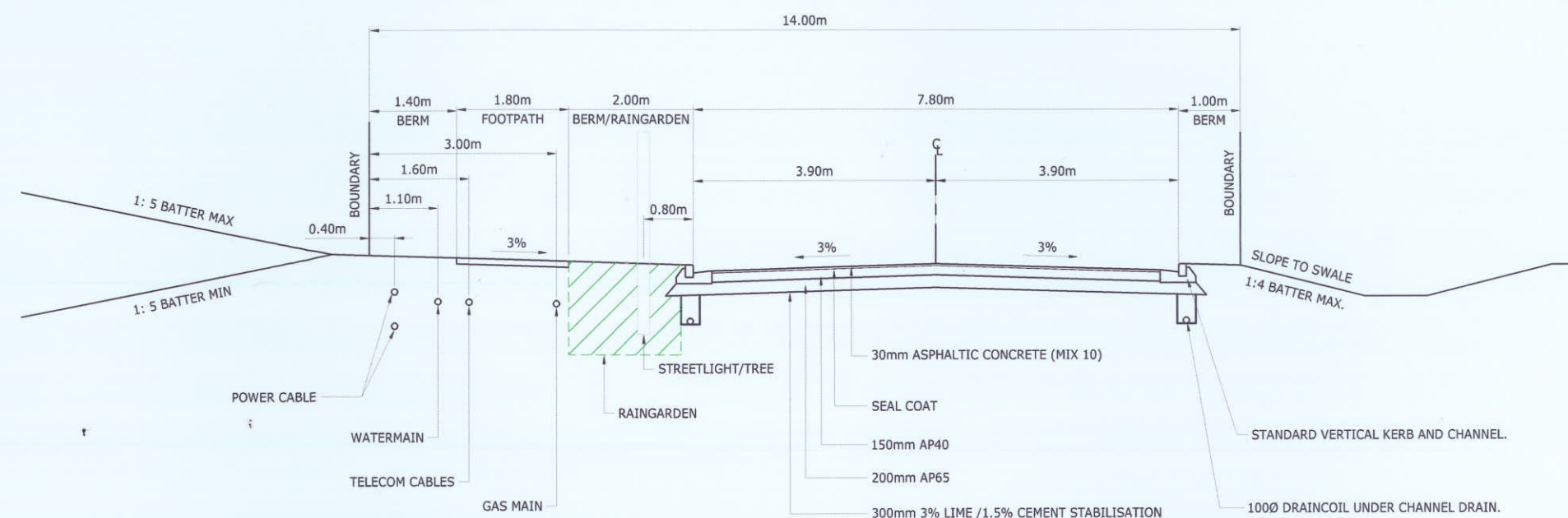
ISSUE STATUS:

AS-BUILT

PROJECT No: 1050-132822-01	SCALES: AS SHOWN	A.
DRAWING No:		REV

136822-AB332	A
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7 TYPICAL CROSS SECTION (PARK EDGE ROAD)  
AB301 SCALE 1:50 -A1 1:100 -A3 ROAD 4 (CH 85 - CH 200.6)

ENGINEERING APPROVAL  
ENG-48683

I CERTIFY THAT THESE ASBUILT PLANS ARE AN ACCURATE RECORD OF THE WORKS UNDERTAKEN AND THAT:  
• THE COORDINATES (X,Y) ARE IN TERMS OF NZTM ON NZGD (2000), AND ARE WITHIN ±50mm.  
• THE LEVELS (Z) ARE IN TERMS OF THE AUCKLAND 1946 (MSL) LINZ DATUM (DOSLI DATUM), AND ARE WITHIN ±25mm.  
Signed: *WJP*  
Date: 30.11.16  
Name: WILLIAM JOHN FREDERICK PLATTS  
Phone: 09-917-5000  
Email: w.platts@harrisonsgrison.com

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W www.harrisonsgrison.com

REF	REVISIONS	BY	DATE
A	AS-BUILT	WJP	30.11.16

PROJECT:  
DONEGAL STUD  
THOMAS ROAD  
FLAT BUSH

TITLE:  
STAGE 8  
PAVEMENT AS-BUILT SECTIONS  
SHEET 4 OF 4

ORIGINATOR:	DATE:	SIGNED:	PLOT BY:
SXK	11.2016		BKB
DRAWN:	DATE:	SIGNED:	PLOT DATE:
BB	11.2016		30.11.16
CHECKED:	DATE:	SIGNED:	SURVEY BY:
SXK	30.11.16		
APPROVED:	DATE:	SIGNED:	SURVEY DATE:
WJP	30.11.16		

ISSUE STATUS: AS-BUILT

PROJECT No:	SCALES:	AS SHOWN	A1
DRAWING No:			REV

136822-AB333 A

## **Appendix B – Classification Test Data**



A TETRA TECH COMPANY

## East Tamaki Laboratory

Coffey Services (NZ) Limited

144A Cryers Road, East Tamaki NZ 2013  
PO Box 58877, Botany, Manukau NZ 2163

Phone: +64 9 272 3375  
Fax: +64 9 272 3378

**Report No: ETAM16S-07279-1**

**Issue No: 1**

# Material Test Report

**Client:** Coffey Services (NZ) Limited (Auckland)  
PO Box 8261, Symonds Street  
Auckland 1150

**Principal:** Hugh Green Group Limited

**Project No.:** GENZETAM01654AC

**Project Name:** GENZAUCK16403AC - DONEGAL STUD STAGE 8

**Lot No.:** N/A **TRN:** N/A

Tests indicated as not accredited are outside the scope of the laboratory's accreditation.  
{This document may not be altered or reproduced except in full. This report relates only to the positions tested.}

**IANZ**  
ACCREDITED LABORATORY

Approved Signatory: Cesar Pura  
(Senior Technician)  
IANZ Accredited Laboratory Number: 105  
Date of Issue: 24/08/2016

## Sample Details

**Sample ID:** ETAM16S-07279

**Client Sample:**

**Date Sampled:** 11/08/2016

**Source:** Unknown (Sampled by Client)

**Material:** Disturbed Soil

**Specification:** No Specification

**Sampling Method:** Unknown (Not IANZ Endorsed)

**Project Location:** Donegal Stud Stage 8

**Sample Location:** HA 08, 0.4 - 0.7 m  
Silty CLAY, highly plastic, pale yellowish gray, moist

## Test Results

Description	Method	Result	Limits
Liquid Limit	NZS 4402:1986 Test 2.2	111	
Plastic Limit	NZS 4402:1986 Test 2.3	Not Tested	
Plasticity Index	NZS 4402:1986 Test 2.4	Not Tested	
Linear Shrinkage	NZS 4402:1986 Test 2.6	23	
Curling		No	
Cracking		Yes	
Sample History		Natural state	
Fraction Tested		Passing 425µm sieve	
Date Tested		22/08/2016	
Moisture Content (%)	NZS 4402:1986 Test 2.1	43.3	
Date Tested		19/08/2016	

## Comments

Sampling Method and Material Description are not IANZ Endorsed as part of this Report.  
Work Order: ETAM16W02676  
Tested By: CP



A TETRA TECH COMPANY

## East Tamaki Laboratory

Coffey Services (NZ) Limited

144A Cryers Road, East Tamaki NZ 2013  
PO Box 58877, Botany, Manukau NZ 2163

Phone: +64 9 272 3375

Fax: +64 9 272 3378

**Report No: ETAM16S-12661-1**

**Issue No: 1**

# Material Test Report

**Client:** Coffey Services (NZ) Limited (Auckland)  
PO Box 8261, Symonds Street  
Auckland 1150

**Principal:** Ray Berry

**Project No.:** 773-ETAM00010AC

**Project Name:** 773-GENZAUCK16403AC - DONEGAL STUD STAGE 8

**Lot No.:** N/A **TRN:** N/A

Tests indicated as not accredited are outside the scope of the laboratory's accreditation.  
{This document may not be altered or reproduced except in full. This report relates only to the positions tested.}



Approved Signatory: James McKelvey  
(Senior Technician)  
IANZ Accredited Laboratory Number: 105  
Date of Issue: 23/11/2016

## Sample Details

**Sample ID:** ETAM16S-12661

**Client Sample:** -

**Date Sampled:** 17/11/2016

**Source:** Unknown (Sampled by Client)

**Material:** Disturbed Soil

**Specification:** No Specification

**Sampling Method:** Unknown (Not IANZ Endorsed)

**Project Location:** Donegal Stud Stage 8, Flat Bush

**Sample Location:** HA12  
0.40 - 0.70 m


## Test Results

Description	Method	Result	Limits
Liquid Limit	NZS 4402:1986 Test 2.2	82	
Plastic Limit	NZS 4402:1986 Test 2.3	Not Tested	
Plasticity Index	NZS 4402:1986 Test 2.4	Not Tested	
Linear Shrinkage	NZS 4402:1986 Test 2.6	17	
Curling		No	
Cracking		No	
Sample History		Natural state	
Fraction Tested		Passing 425µm sieve	
Date Tested		21/11/2016	
Moisture Content (%)	NZS 4402:1986 Test 2.1	39.3	
Date Tested		17/11/2016	

## Comments

Work Order: ETAM16W03780  
Tested By: CP

## **Appendix C - Field Density Test Summary Sheets**

<b>Client:</b> Coffey Geotechnics NZ Ltd <b>Address</b> PO Box 8261, Symonds Street, Auckland 1150 <b>Attention:</b> Ray Berry <b>c.c:</b> - <b>Project:</b> GENZAUCK16403AC - DONEGAL STUD STAGE 8  <b>Location:</b> Flat Bush										<div><div>PROJECT CODE:GENZETAM00881AC - 00</div><div>Revision No. 1</div></div> <div><div><div>IANZ</div><div>ACCREDITED LABORATORY</div></div><div>Tests indicated as not accredited are outside the scope of the laboratory's accreditation</div><div><div></div><div>Approved Signatory: Eric Paton</div><div>Issue date: 26/09/16</div></div></div>											
Test method: Test Methods in accordance with: Shear Strength (using field Shear vane in accordance with NZGS 2001):Nuclear Densometer Testing (in accordance with NZS 4407:2015 Test 4.2): Water Content Testing (in accordance with NZS 4402:1986 Test 2.1): Density Calculations (in accordance with NZS 4402:1986 Tests 4.1.1.5(b)). Please note that Air Void calculations are not IANZ endorsed as part of this report.																					
Date	Work Order No:	Tested by	Test No.	Layer	Material tested	Location	Easting	Northing	RL	Test Depth (mm) FL = Finished level	Comments	Field Shear Strength in kPa UTP = Unable to penetrate				Wet Density (t/m <sup>3</sup> )	Oven Water Content (%)	Dry Density (tm <sup>3</sup> )	Solid Density	Air Voids (%)	
25/02/16	ETAM16W00599	AB	1	Fill	Clay	Road Fill	1769947	5905444	46.50			UTP	UTP	UTP	UTP	1.91	21.7	1.57	2.70	7.8	
25/02/16	ETAM16W00599	AB	2	Fill	Clay	Road Fill	1769938	5905367	-			UTP	UTP	UTP	UTP	1.97	20.8	1.63	2.70	5.6	
26/02/16	ETAM16W00600	OT	3	Fill	Silty CLAY	See plan	1769990	5905347	-			198	216+	187	216+	1.92	21.8	1.58	2.70	7.0	
26/02/16	ETAM16W00600	OT	4	Fill	Silty CLAY	See plan	1769984	5905367	-			133	133	187	163	1.99	24.7	1.60	2.70	1.3	
26/02/16	ETAM16W00600	OT	5	Fill	Silty CLAY	See plan	1769937	5905337	-			216+	216+	216+	216+	2.01	24.2	1.62	2.70	0.8	
07/03/16	ETAM16W00676	DL	6	Fill	Clay	General fill	1769990	5905358	-			239+	239+	239+	239+	1.97	24.5	1.58	2.70	2.6	
07/03/16	ETAM16W00676	DL	7	Fill	Clay	General fill	1769989	5905323	-		*Field nuc water content applied	239+	239+	239+	239+	2.03	*22.3	1.66	2.70	1.5	
08/03/16	ETAM16W00696	DL	8	Fill	Clay	General fill	1769905	5905349	-			239+	239+	239+	239+	1.88	30.3	1.44	2.70	3.0	
08/03/16	ETAM16W00696	DL	9	Fill	Clay	General fill	1769895	5905366	-			239+	239+	239+	239+	1.93	27.9	1.51	2.70	2.1	
10/03/16	ETAM16W00782	DL	10	Fill	Clay	General fill	1769890	5905345	-			239+	239+	239+	239+	1.88	24.3	1.51	2.70	7.2	
10/03/16	ETAM16W00782	DL	11	Fill	Clay	General fill	1769871	5905365	-			239+	239+	239+	239+	2.00	27.3	1.57	2.70	0.0	
10/03/16	ETAM16W00782	DL	12	Fill	Clay	General fill	1769912	5905346	-			239+	239+	239+	239+	2.04	30.6	1.57	2.70	0.0	
14/03/16	ETAM16W00886	DL	13	Fill	Clay	General fill	1769928	5905395	-			208	182	156	145	2.09	27.1	1.64	2.70	0.0	
14/03/16	ETAM16W00886	DL	14	Fill	Clay	General fill	1769907	5905371	-			228	212	187	152	2.01	34.0	1.50	2.7	0.0	
14/03/16	ETAM16W00886	DL	15	Fill	Clay	General fill	1769889	5905378	-			152	228	182	182	2.00	26.5	1.58	2.7	0.0	
15/03/16	ETAM16W00889	DL	16	Fill	Clay	General fill	1769932	5905333	-			239+	239+	239+	239+	1.99	22.7	1.62	2.7	3.1	
15/03/16	ETAM16W00889	DL	17	Fill	Clay	General fill	1769943	5905393	-			239+	239+	239+	239+	1.96	21.8	1.61	2.7	5.3	
15/03/16	ETAM16W00889	DL	18	Fill	Clay	General fill	1769957	5905412	-			239+	239+	239+	239+	1.94	27.0	1.52	2.7	2.4	
17/03/16	ETAM16W00891	DL	19	Fill	Clay	General fill	1770044	5905517	-	300mm to subgrade		239+	239+	239+	239+	1.99	22.2	1.63	2.7	3.8	
17/03/16	ETAM16W00891	DL	20	Fill	Clay	General fill	1770036	5905507	-	FL		239+	239+	239+	239+	2.04	18.2	1.72	2.7	4.8	
30/03/16	ETAM16W01000	DL	21	Fill	Clay	Refer to plan	1770039	5905304	-			124	148	184	111	1.74	24.9	1.39	2.7	13.8	
30/03/16	ETAM16W01000	DL	22	Fill	Clay	Refer to plan	1770028	5905315	-			196+	196+	196+	196+	1.99	24.9	1.60	2.7	1.2	
30/03/16	ETAM16W01000	DL	23	Fill	Clay	Refer to plan	1769995	5905314	-			196+	196+	196+	196+	1.96	24.5	1.57	2.7	3.2	



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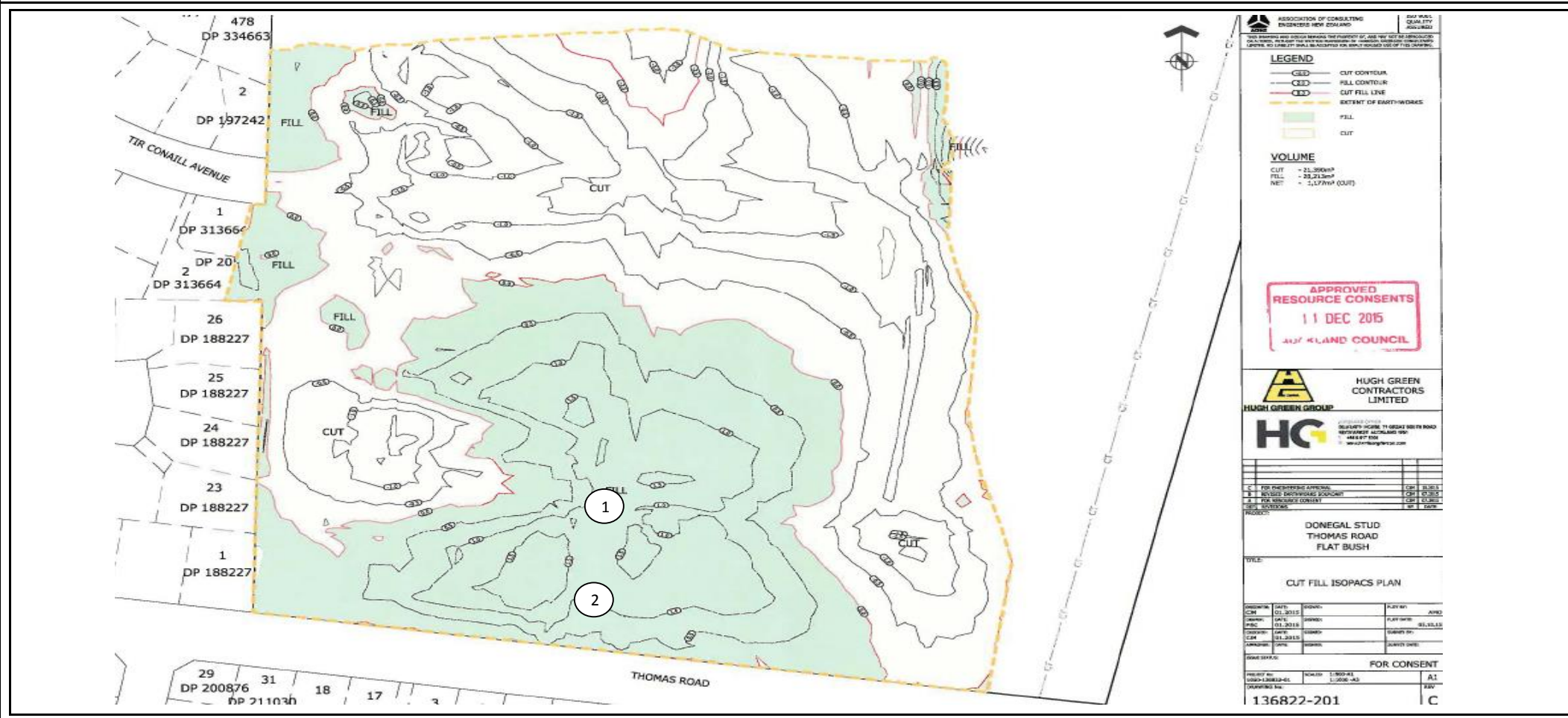
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**Project:** GENZAUCK16403AC - DONEGAL STUD STAGE 8

**Location:** Road fill

**Tested by:** AB  
**Date tested:** 25/02/16



## SITE PLAN

NOT TO SCALE

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Work Order No: ETAM16W00600

Page: 3 of 10

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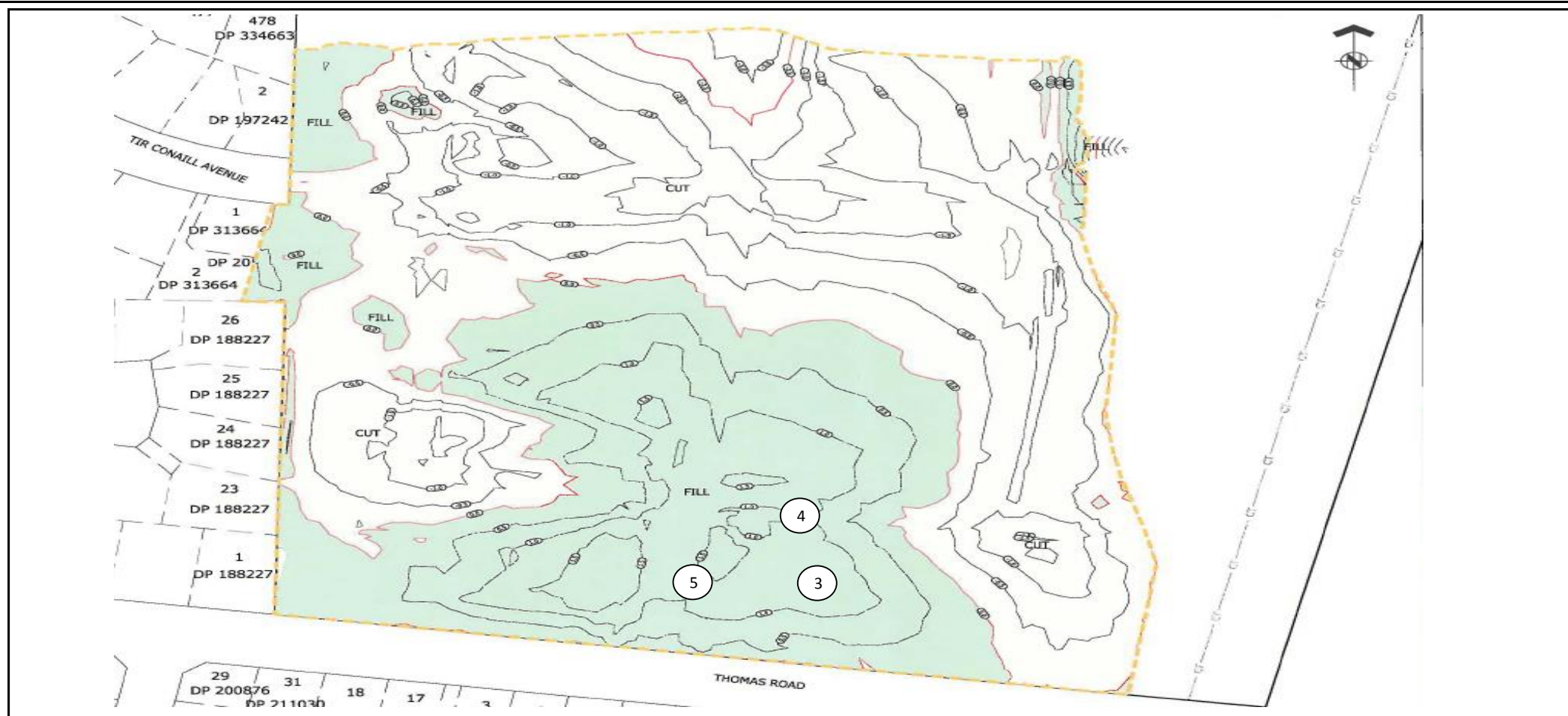
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Tested by:

OT

Date tested:

26/02/16





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Page: 4 of 10

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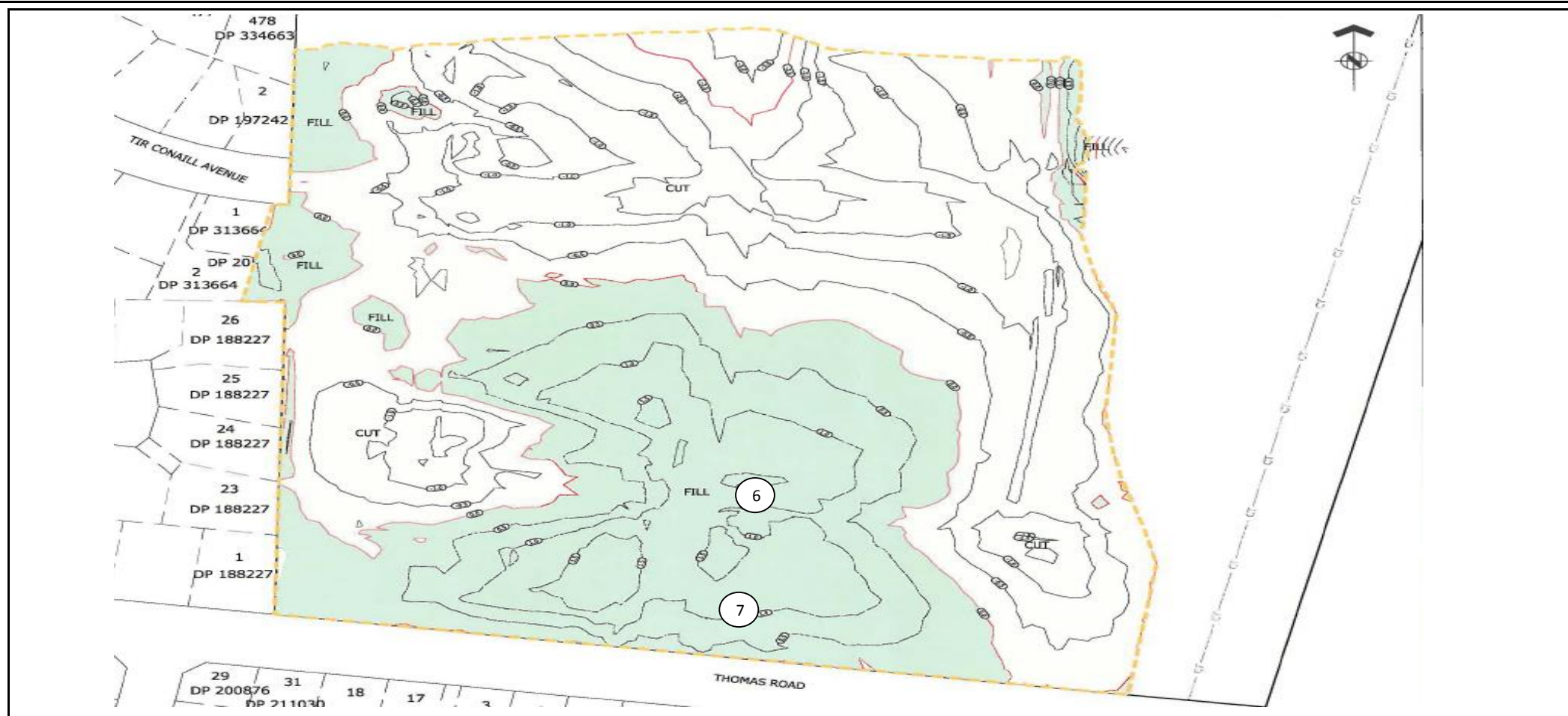
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Tested by:

DL

Date tested:

07/03/16



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Page: 5 of 10

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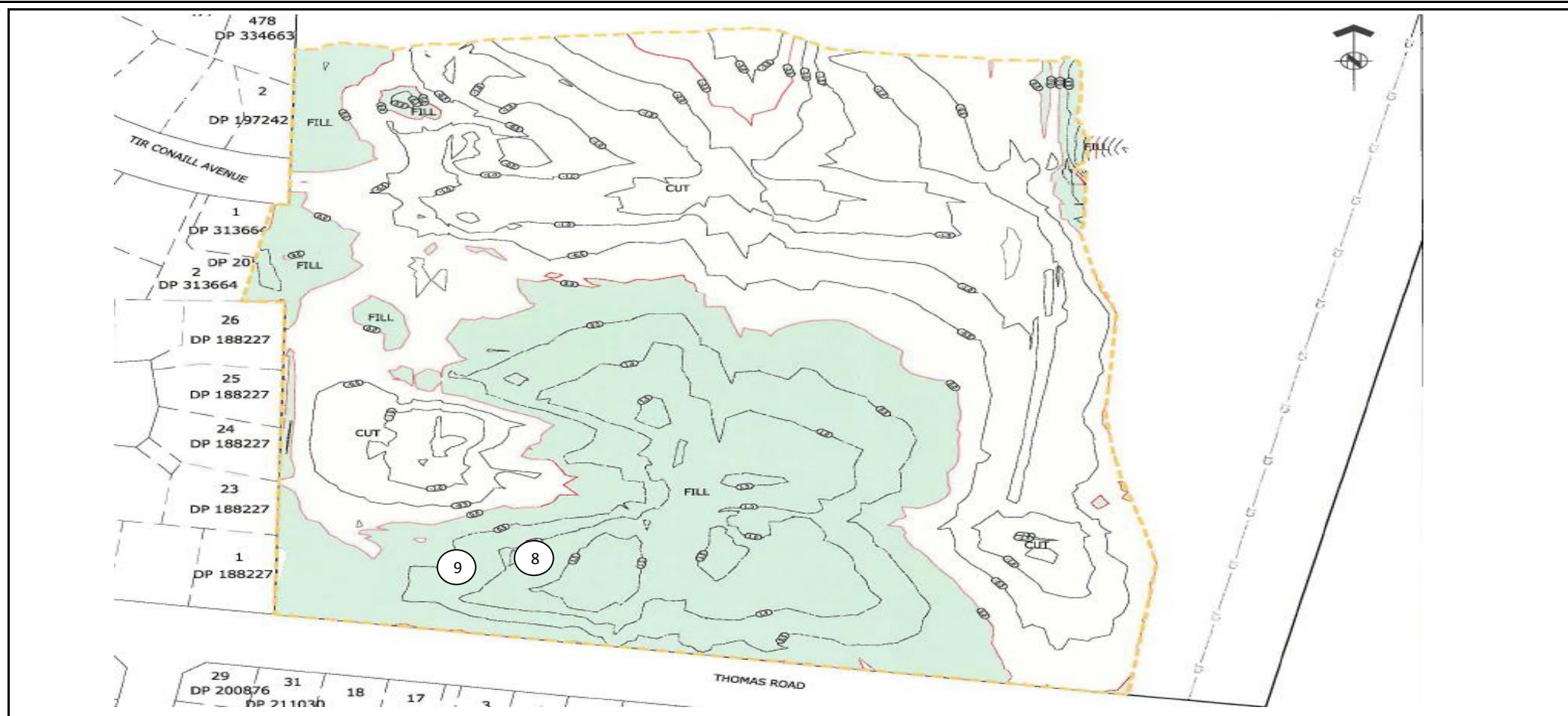
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Tested by:

DL

Date tested:

08/03/16



## SITE PLAN

NOT TO SCALE

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Page: 6 of 10

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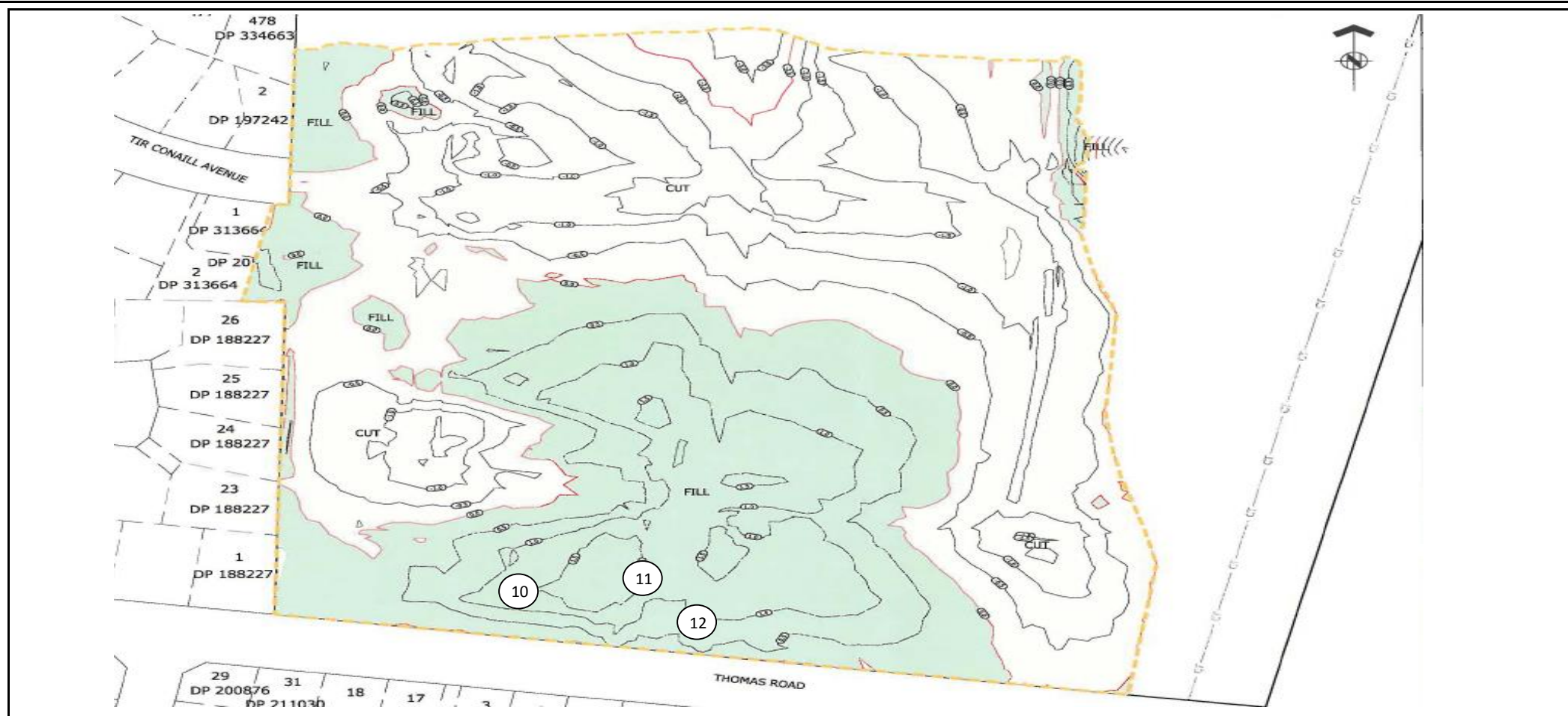
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Tested by:

DL

Date tested:

10/03/16





## SITE PLAN

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Page: 7 of 10

**Project:** GENZAUCK16403AC - DONEGAL STUD STAGE 8

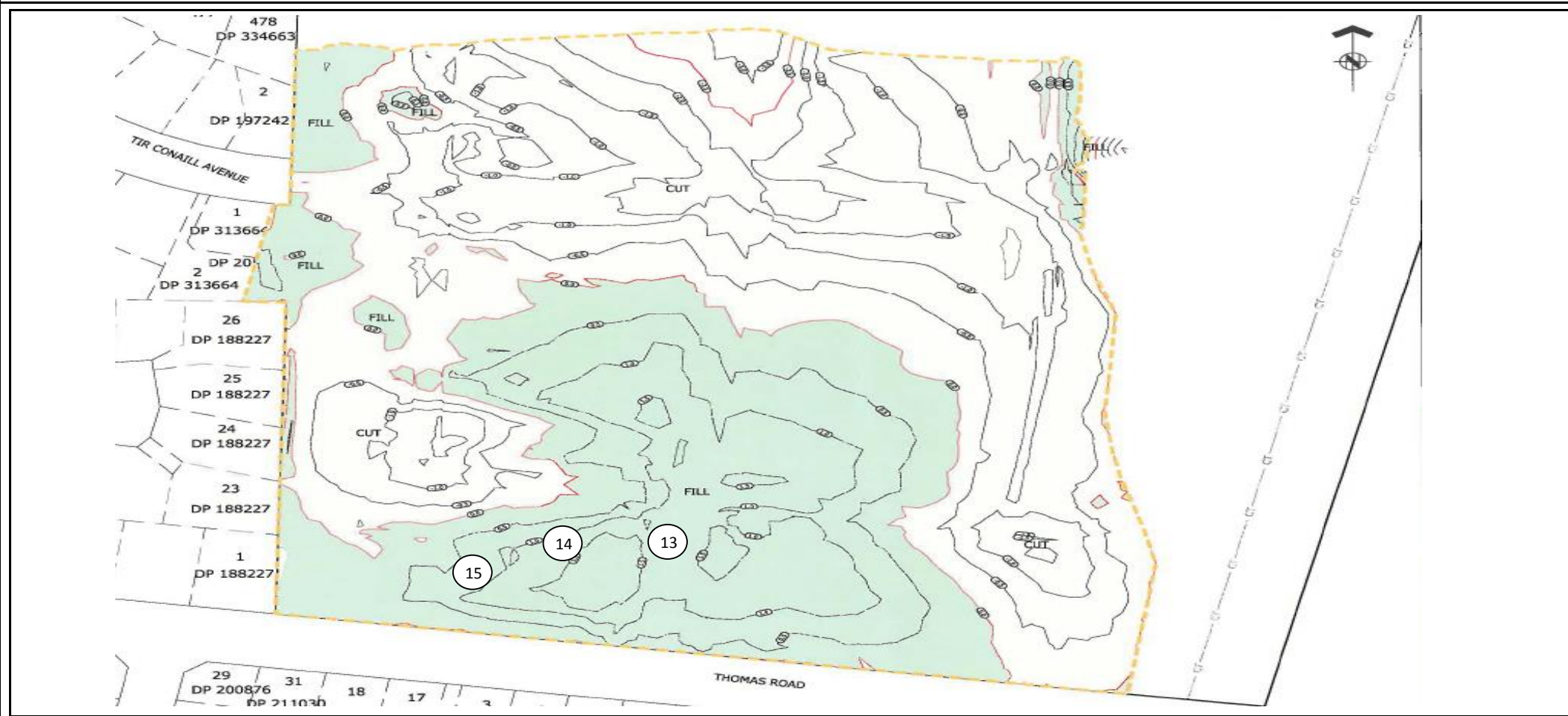
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Tested by:

DL

Date tested:

14/03/16



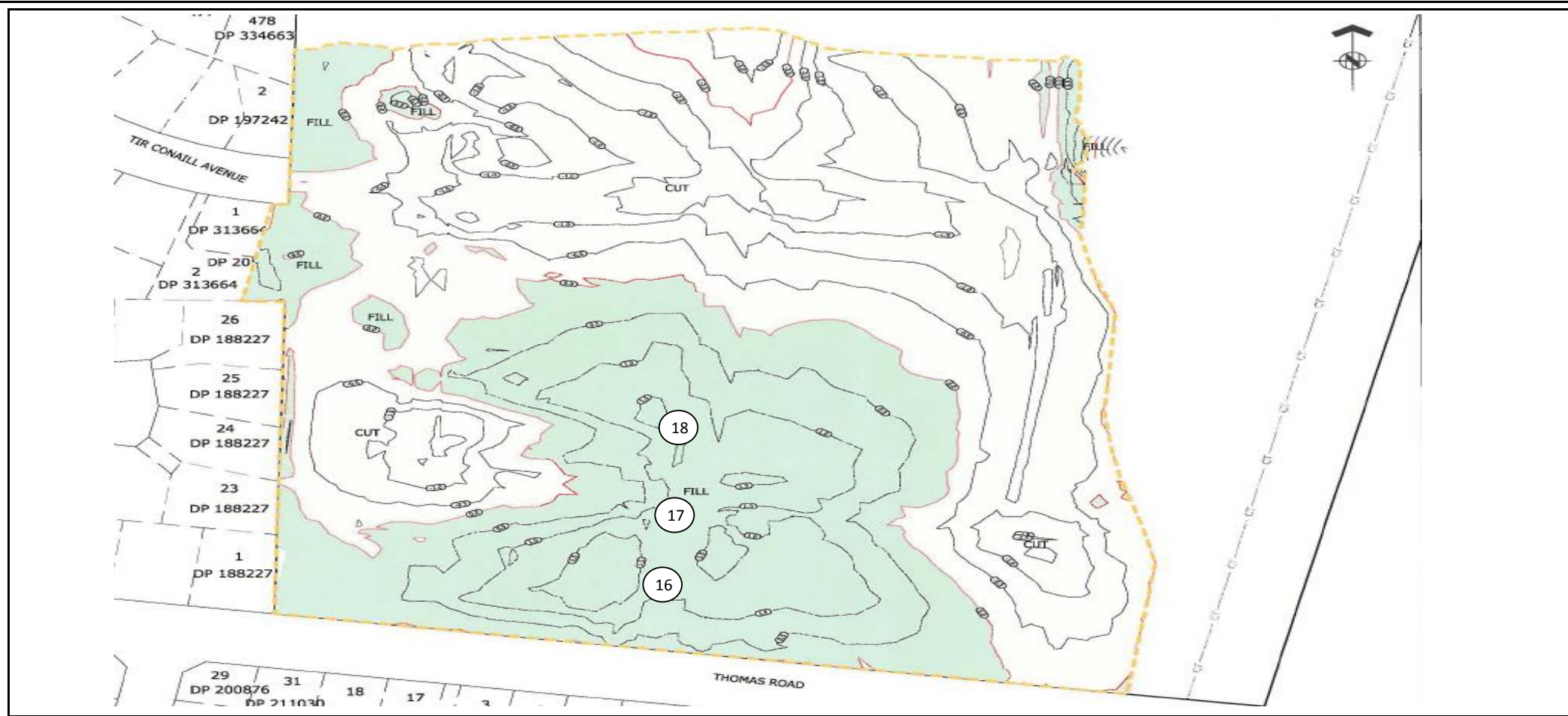
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Work Order No: ETAM16W00889

Page: 8 of 10

Tested by: DL

Date tested: 15/03/16



## SITE PLAN

NOT TO SCALE

**Project No: GENZETAM00881AC - 00**

Work Order No: ETAM16W00891

Page: 9 of 10

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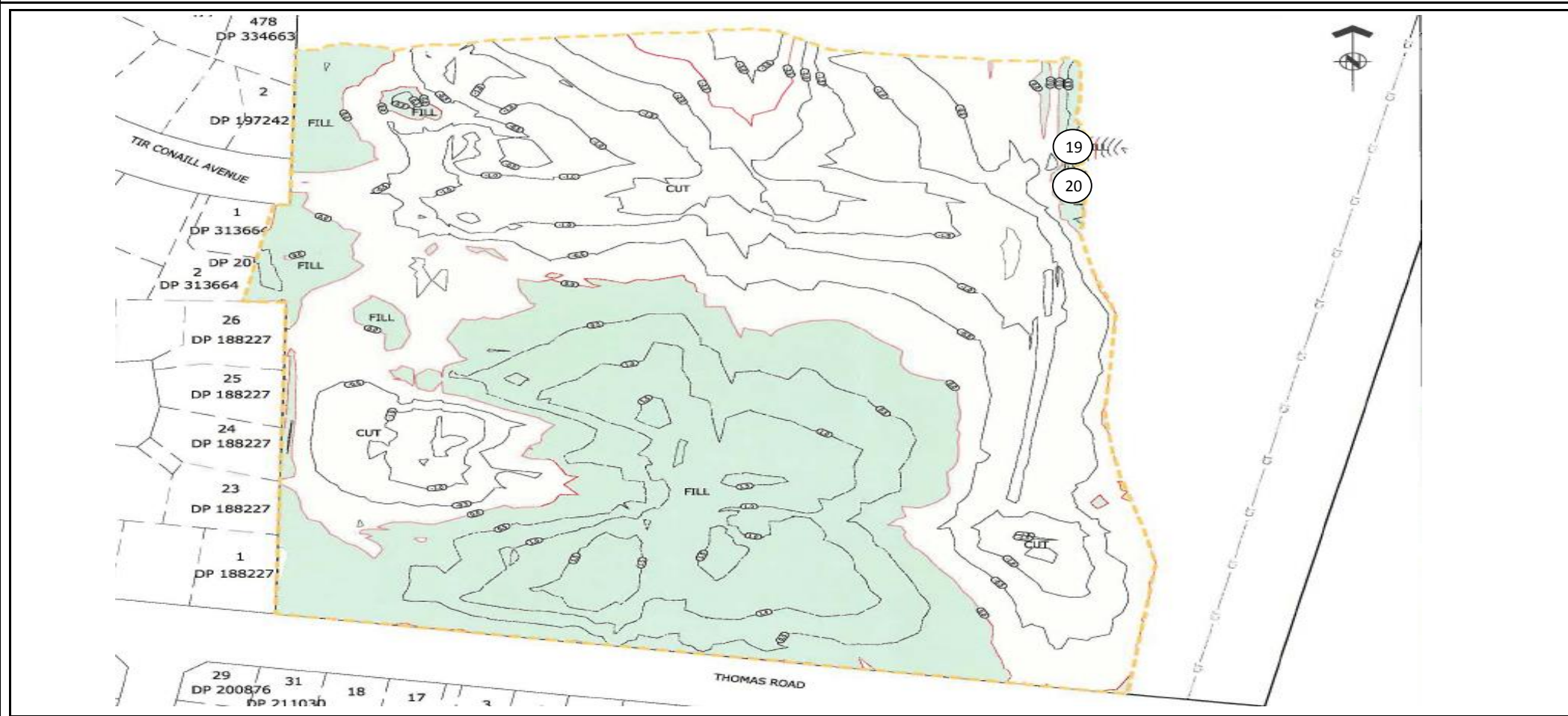
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Tested by:

DL

Date tested:

17/03/16





## SITE PLAN

NOT TO SCALE

**Project No: GENZETAM00881AC - 00**

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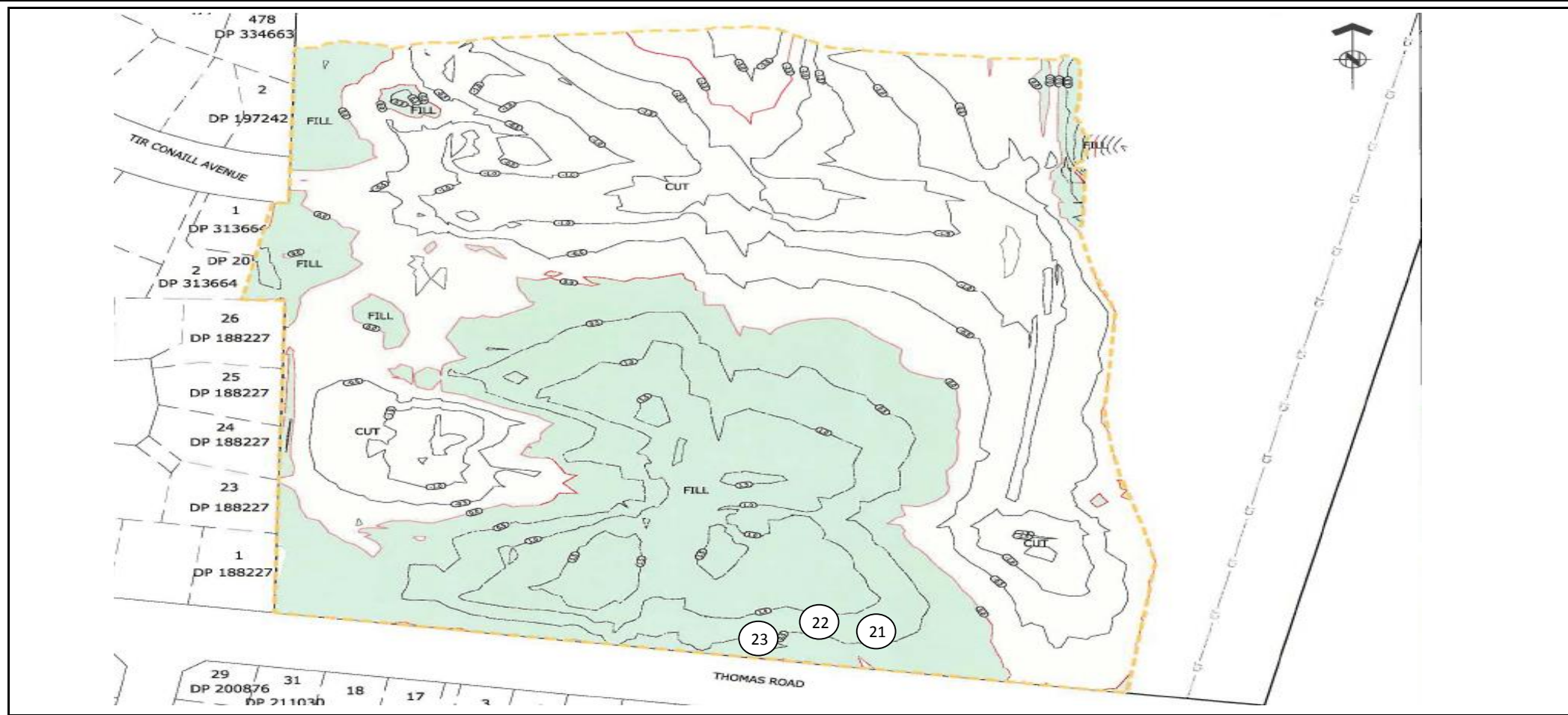
**Location:** As below



Tested by:

DL

Date tested:

30/03/16



<b>Client:</b> Coffey Services NZ Ltd (Auckland) <b>Address:</b> PO Box 8261, Symonds Street, Auckland 1150 <b>Attention:</b> Ray Berry <b>c.c.:</b> - <b>Project:</b> 773-GENZAUCK16403AC - DONEGAL STUD STAGE 8  <b>Location:</b> Previous Project No. = GENZETAM00818AC	<b>PROJECT CODE:</b> 773-ETAM00010AC <b>Page:</b> 1 of 2																																																		
<div style="display: flex; justify-content: space-around; align-items: center;"> <div style="text-align: center;">   <b>IANZ</b>  <small>ACCREDITED LABORATORY</small> </div> <div style="text-align: center;"> <small>Tests indicated as not accredited are outside the scope of the laboratory's accreditation</small> </div> <div style="text-align: center;">   <b>Approved Signatory:</b> James McKelvey  <b>Issue date:</b> 2/12/2016         </div> </div>																																																			
<b>Test method:</b> Test Methods in accordance with: Shear Strength (using field Shear vane in accordance with NZGS 2001); Nuclear Densometer Testing (in accordance with NZS 4407:2015 Test 4.2); Water Content Testing (in accordance with NZS 4402:1986 Test 2.1); Density Calculations (in accordance with NZS 4402:1986 Tests 4.1.1.5(b)). Please note that Air Void calculations are not IANZ endorsed as part of this report.																																																			
<table border="1" style="width: 100%; border-collapse: collapse; font-size: x-small;"> <thead> <tr style="background-color: #e6f2ff;"> <th>Date</th> <th>Work Order No:</th> <th>Tested by</th> <th>Test No.</th> <th>Layer</th> <th>Material tested</th> <th>Location</th> <th>Chainage (m)</th> <th>Offset (m)</th> <th>Offset from</th> <th>Easting</th> <th>Northing</th> <th>Lane</th> <th>RL</th> <th>Test Depth (mm) FL = Finished level</th> <th>Comments</th> <th colspan="4">Field Shear Strength in kPa UTP = Unable to penetrate</th> <th>Wet Density (t/m<sup>3</sup>)</th> <th>Oven Water Content (%)</th> <th>Dry Density (t/m<sup>3</sup>)</th> <th>Solid Density (t/m<sup>3</sup>)</th> <th>Air Voids (%)</th> </tr> </thead> <tbody> <tr> <td>30/11/2016</td> <td>ETAM16W04109</td> <td>FP + JBG</td> <td>24</td> <td>FL</td> <td>Silty CLAY</td> <td>General Fill</td> <td>-</td> <td>-</td> <td>-</td> <td>1770036</td> <td>5905315</td> <td>-</td> <td>-</td> <td>150</td> <td>Retest of #21</td> <td>UTP</td> <td>UTP</td> <td>UTP</td> <td>UTP</td> <td>1.89</td> <td>24.4</td> <td>1.52</td> <td>2.70</td> <td>6.8</td> </tr> </tbody> </table>		Date	Work Order No:	Tested by	Test No.	Layer	Material tested	Location	Chainage (m)	Offset (m)	Offset from	Easting	Northing	Lane	RL	Test Depth (mm) FL = Finished level	Comments	Field Shear Strength in kPa UTP = Unable to penetrate				Wet Density (t/m <sup>3</sup> )	Oven Water Content (%)	Dry Density (t/m <sup>3</sup> )	Solid Density (t/m <sup>3</sup> )	Air Voids (%)	30/11/2016	ETAM16W04109	FP + JBG	24	FL	Silty CLAY	General Fill	-	-	-	1770036	5905315	-	-	150	Retest of #21	UTP	UTP	UTP	UTP	1.89	24.4	1.52	2.70	6.8
Date	Work Order No:	Tested by	Test No.	Layer	Material tested	Location	Chainage (m)	Offset (m)	Offset from	Easting	Northing	Lane	RL	Test Depth (mm) FL = Finished level	Comments	Field Shear Strength in kPa UTP = Unable to penetrate				Wet Density (t/m <sup>3</sup> )	Oven Water Content (%)	Dry Density (t/m <sup>3</sup> )	Solid Density (t/m <sup>3</sup> )	Air Voids (%)																											
30/11/2016	ETAM16W04109	FP + JBG	24	FL	Silty CLAY	General Fill	-	-	-	1770036	5905315	-	-	150	Retest of #21	UTP	UTP	UTP	UTP	1.89	24.4	1.52	2.70	6.8																											



## SITE PLAN

NOT TO SCALE

**Project No: 773-ETAM00010AC**

Work Order No: ETAM16W04109

Page: 2 of 2

**Project:** 773-GENZAUCK16403AC - DONEGAL STUD STAGE 8

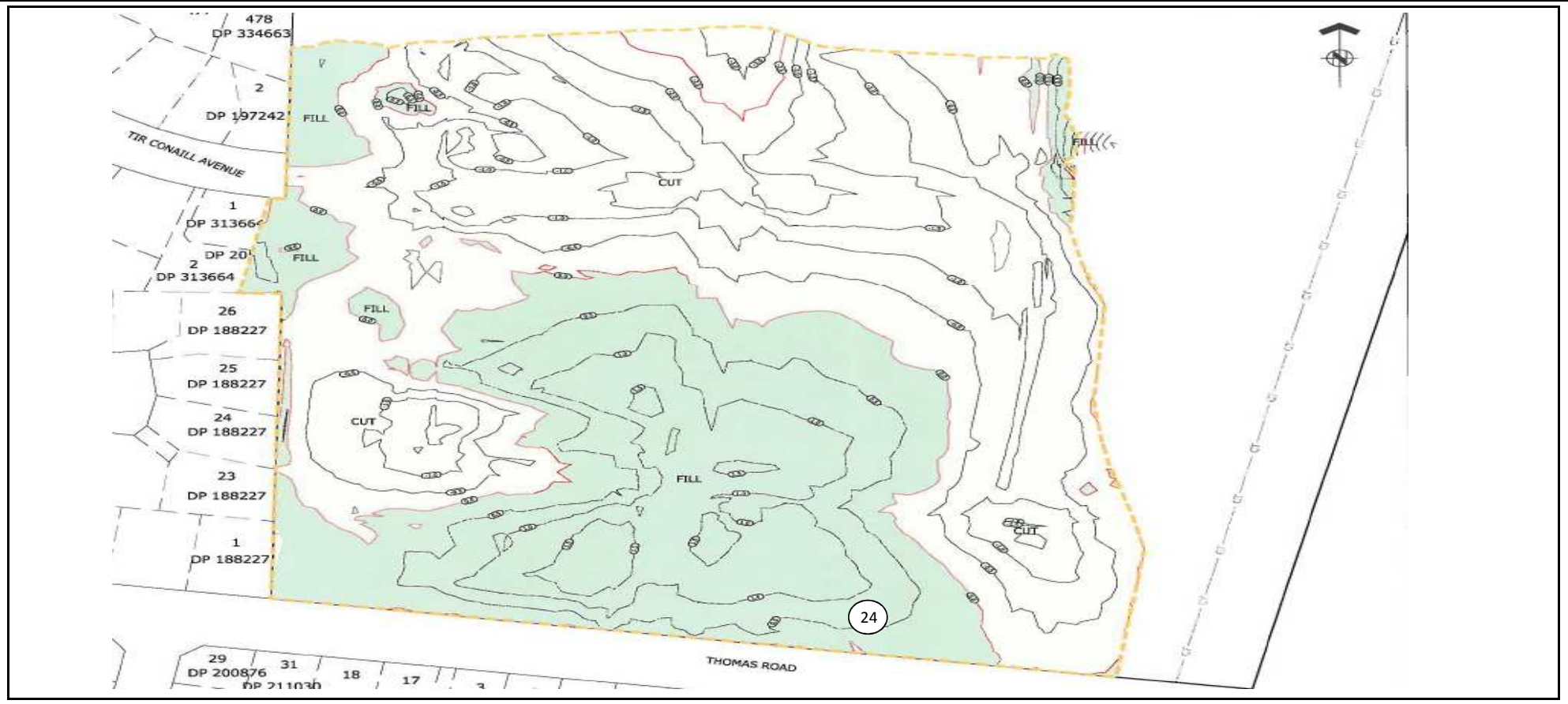
**Location:** As below

Tested by:

FP and JBG

Date tested:

30/11/2016



## **Appendix D – Previous Earthworks Certification Documentation**

**APPENDIX 1**  
**SCALA PENETROMETER TEST RESULTS**

# geolab

air, soil & water  
laboratory services

P.O.Box 5760, WELLESLEY STREET.

PHONE: (09) 3090346

## SCALA PENETROMETER TEST

SITE: DONAGAL STUD FARM, EAST TAMAKI

JOB No: 147515.1

CLIENT: GREEN AND McCAHILL

DATE TESTED: 22/1/98

DRAWING No: 7515.SC9.DWG

TABLE OF BLOWS PER 50mm INCREMENT

DEPTH OF PENETRATION	SC 1	SC 2	SC 3	SC 4	SC 5	SC 6	SC 7	SC 8	SC 9	SC 10
DEPTH START (M)	0.00m	0.00m	0.00m	0.00m	0.00m	0.00m	0.00m	0.00m	0.00m	0.00m
50mm	1	1	1	1	1	1	1	1	1	1
100mm	2	1	1	1	1	1	1	2	1	1
150mm	2	1	3	1	1	2	3	3	2	3
200mm	3	2	2	1	2	5	2	3	4	2
250mm	4	1	1	1	1	4	2	2	5	2
300mm	5	2	1	2	2	4	3	1	4	3
350mm	5	2	1	1	1	4	3	1	7	1
400mm	4	1	2	1	2	3	3	1	3	2
450mm	4	1	2	1	1	3	3	1	4	2
500mm	4	1	1	1	2	4	4	4	4	1
550mm	3	1	1	2	1	3	3	3	3	2
600mm	4	1	1	4	2	2	3	3	2	2
650mm	4	1	1	4	2	2	4	1	2	4
700mm	4	1	1	4	2	1	2	1	2	3
750mm	7	1	1	2	2	2	2	1	2	4
800mm	20+	1	2	3	2	2	2	1	2	3
850mm		1	2	2	4	2	2	2	3	4
900mm		1	2	1	7	2	2	1	2	3
950mm		1	1	1	2	2	2	1	2	4
1000mm		1	1	1	2	2	2	3	3	2
1050mm		1	1	1	2	1	1	2	4	2
1100mm		2	1	1	2	3	2	2	4	2
1150mm		2	2	2	2	3	3	3	4	3
1200mm		2	2	2	2	2	3	3	5	4
1250mm		4	3	2	3	6	3	5	3	2
1300mm		5	2	2	4	6	3	3	5	3
1350mm		9	4	3	4	4	3	5	5	4
1400mm		11	4	2	5	4	3	4	5	3
1450mm		12	3	5	5	3	5	4	8	4
1500mm		12	4	4	4	3	5	4	3	4
1550mm										
1600mm										
1650mm										
1700mm										
1750mm										
1800mm										
1850mm										
1900mm										
1950mm										
2000mm										
DEPTH END (M)	0.80m	1.50m	1.50m	1.50m	1.50m	1.50m	1.50m	1.50m	1.50m	1.50m

COMMENTS:

# geolab

air, soil & water  
laboratory services

P.O.Box 5760, WELLESLEY STREET.

PHONE: (09) 3090346

## SCALA PENETROMETER TEST

SITE: DONAGAL STUD FARM, EAST TAMAKI

JOB No: 147515.1

CLIENT: GREEN AND McCAHILL

DATE TESTED: 22/1/98

DRAWING No: 7515-SC10.DWG

TABLE OF BLOWS PER 50mm INCREMENT

DEPTH OF PENETRATION	SC 11	SC 12	SC 13	SC 14	SC 15	SC 16	SC 17	SC 18	SC 19	SC 20
DEPTH START (M)	0.00m	0.00m	1.00m	0.00m	0.00m	0.00m	0.00m	0.00m	0.00m	0.00m
50mm	1	1	1	1	1	1	1	1	1	1
100mm	1	1	1	1	1	2	3	1	1	1
150mm	1	1	1	1	2	4	4	3	5	1
200mm	1	1	2	1	1	4	4	3	4	1
250mm	1	1	2	1	2	4	4	3	3	1
300mm	1	1	3	1	2	4	4	3	2	1
350mm	2	1	5	1	5	9	7	4	1	1
400mm	3	1	7	1	3	5	7	4	2	1
450mm	1	1	5	1	7	2	4	4	2	1
500mm	1	1	6	1	5	2	4	4	2	1
550mm	2	1	7	1	3	2	2	3	2	1
600mm	2	4	6	1	3	2	2	3	2	1
650mm	4	4	5	2	3	2	1	3	2	2
700mm	6	2	5	2	3	2	2	3	1	1
750mm	6	2	5	1	2	1	3	4	2	1
800mm	4	2	6	2	3	2	4	4	1	1
850mm	3	2	5	1	2	2	3	5	2	1
900mm	4	2	3	2	2	2	2	2	1	1
950mm	6	1	1	1	2	1	2	1	2	1
1000mm	3	1	1	1	3	2	2	1	1	1
1050mm	2	1	2	1	4	2	2	4	3	1
1100mm	1	1	2	1	3	3	4	3	3	1
1150mm	2	2	1	1	2	4	6	2	3	1
1200mm	3	2	1	1	3	3	9	2	3	1
1250mm	4	4	3	2	2	3	9	3	2	1
1300mm	2	2	3	1	3	2	9	3	2	1
1350mm	3	2	2	1	4	3	9	3	2	1
1400mm	3	2	2	1	4	3	9	4	2	3
1450mm	3	2	2	2	5	5	9	4	2	4
1500mm	3	2	2	1	5	5	8	4	2	6
1550mm										
1600mm										
1650mm										
1700mm										
1750mm										
1800mm										
1850mm										
1900mm										
1950mm										
2000mm										
DEPTH END (M)	1.50m	1.50m	1.50m	1.50m	1.50m	1.50m	1.50m	1.50m	1.50m	1.50m

COMMENTS:

# geolab

air, soil & water  
laboratory services

P.O.Box 5760, WELLESLEY STREET.

PHONE: (09) 3090346

## SCALA PENETROMETER TEST

SITE: DONAGAL STUD FARM, EAST TAMAKI

JOB No: 147515.1

CLIENT: GREEN AND McCAHILL

DATE TESTED: 22/1/98

DRAWING No: 7515-SC11.DWG

TABLE OF BLOWS PER 50mm INCREMENT

DEPTH OF PENETRATION	SC 21	SC 22	SC 23						
DEPTH START (M)	0.00m	0.00m	0.00m						
50mm	1	1	1						
100mm	1	2	1						
150mm	2	4	3						
200mm	2	2	2						
250mm	1	2	4						
300mm	1	2	5						
350mm	1	5	6						
400mm	2	3	4						
450mm	3	3	4						
500mm	11	3	2						
550mm	7	4	3						
600mm	4	2	2						
650mm	4	2	4						
700mm	3	2	5						
750mm	2	3	9						
800mm	2	5	6						
850mm	2	10	6						
900mm	1	10	3						
950mm	1	9	3						
1000mm	1	10	3						
1050mm	1	9							
1100mm	2	10							
1150mm	2	10							
1200mm	2	9							
1250mm	2	10							
1300mm	2	20+							
1350mm	3								
1400mm	4								
1450mm	4								
1500mm	3								
1550mm									
1600mm									
1650mm									
1700mm									
1750mm									
1800mm									
1850mm									
1900mm									
1950mm									
2000mm									
DEPTH END (M)	1.50m	1.30m	1.00m						

COMMENTS:

**APPENDIX 2**  
**COMPACTION CONTROL TEST RESULTS**

## INSITU DENSITY TEST RESULTS

SITE: DONAGAL STUD, CHAPPLE ROAD

JOB No: 147515.2

TEST NO	DATE	R.L.	SOIL DESCRIPTION	Pb	M.C.	Pd	S.G.	A.V.	SHEAR STRENGTH	RETEST No	COMMENTS
T1	12/11/97		Silt, very clayey, grey, some brown	1867	30.6	1429	2.68	2.9	V,191+x2,174		
T2	21/11/97		Silt, clayey, pale grey, light brown pockets	1864	30.6	1427	2.68	3.1	154,143,125		
T3			Silt, clayey, pale grey, light brown pockets	1681	42.6	1179	2.68	5.8	V,192+x3,145		
T4			Silt, clayey, pale grey, light brown pockets	1682	42.6	1180	2.68	5.7	140,134		
T5	24/11/97		Silt, clayey, pale grey, light brown pockets	1724	48.3	1163	2.68	0.5	V,153,134,126	T9	Mixed to blend and dry before recompacting
T6			Silt, clayey, pale grey, light brown pockets	1725	48.3	1163	2.68	0.4	111,95,84		
T7			Silt, slightly clayey, light brown, occasional light grey	1813	35.9	1334	2.68	2.4	V,192+x5,145		
T8			Silt, slightly clayey, light brown, occasional light grey	1812	35.9	1334	2.68	2.4			
T9			Silt, slightly clayey, light brown, occasional light grey	1964	24.2	1582	2.68	2.7	V,174+x4,143,127		
T10	26/11/97		Silt, slightly clayey, trace sand (fg) light brown	1963	24.2	1581	2.68	2.8	V,174+x5,130	T3	
T11			Silt, slightly clayey, trace sand (fg) light brown	1964	29.9	1511	2.68	-1.7			
T12	27/11/97		Silt, trace sand (f-mg), light brown	1967	29.9	1514	2.68	-1.8			
				2000	23.4	1620	2.68	1.6	V,174+x2,166,152		
				1998	23.4	1619	2.68	1.7	143,136		
				1944	24.5	1561	2.68	3.5	V,174+x4,140		
				1940	24.5	1558	2.68	3.7	127		
				1628	52.9	1065	2.68	4.0	V,174+x6		
				1630	52.9	1066	2.68	3.8			
				1920	17.0	1641	2.68	10.9	V,174+x3,143,132		
				1923	17.0	1644	2.68	10.7	121		
				1825	34.4	1358	2.68	2.7	V,174+x3,143,121		
				1826	34.4	1359	2.68	2.6	119		
				1705	39.8	1219	2.68	5.9	V,192192+x6		
				1706	39.8	1220	2.68	5.9			

Pb Bulk Density (kg/m<sup>3</sup>)  
 M.C. Moisture Content (%)  
 Pd Dry Density (kg/m<sup>3</sup>)  
 A.V. Air Voids (%)

S Shear Strength (P - blows per 50mm on scala penetrometer,  
 V - shear strength by vane (kPa) in terms of BS: 1377:1975)  
 S.G. Specific Gravity  
 R.L. Reduced Level (metres)



## INSITU DENSITY TEST RESULTS

SITE: DONAGAL STUD, CHAPPLE ROAD

JOB No: 147515.2

TEST NO	DATE	R.L.	SOIL DESCRIPTION	Pb	M.C.	Pd	S.G.	A.V.	SHEAR STRENGTH	RETEST No	COMMENTS
T13			Silt, slightly clayey, light brown and light grey	2015	21.5	1659	2.68	2.5	V, 192+x2, 163, 144	T14	Excavated to 0.3m and left to dry before recompacting
T14	28/11/97		Silt, slightly clayey, light brown trace topsoil	2014	21.5	1658	2.68	2.5	132, 100	T13	
T15	01/12/97		Silt, slightly clayey, light brown and light grey	2009	23.5	1627	2.68	1.1	V, 174+x2, 158, 148		
T16			Silt, slightly clayey, light brown and light grey	2008	23.5	1626	2.68	1.2	140, 122		
T17	05/12/97		Silt, slightly clayey, light brown and grey and clayey, light grey and grey brown, moist to wet	1856	29.2	1436	2.68	4.4	V, 192+x2, 158		
T18	08/12/97		Silt, slightly clayey, brown and light brown	1854	29.2	1434	2.68	4.5	145x2, 122		
T19			Silt, slightly clayey, brown	1760	25.7	1400	2.68	11.8	V, 192+x3, 165, 158		
T20			Silt, slightly clayey, brown	1762	25.7	1402	2.68	11.7	151		
T21			Silt, slightly clayey, light grey and orange/red	1695	65.0	1027	2.68	-5.1	V, 120, 104, 94, 75	T23	
T22	09/12/97		Silt, slightly clayey, brown and light brown	1697	65.0	1028	2.68	-5.2	64, 62		
T23			Silt, slightly clayey, light grey and black-brown	1724	50.7	1144	2.68	-0.7	V, 191+x2, 178, 168		
T24	11/12/97		Silt, slightly clayey, light brown and light grey	1725	50.7	1145	2.68	-0.7	136, 128		
				1798	32.6	1356	2.68	5.2	V, 191+x6		
				1790	32.6	1350	2.68	5.6			
				1738	31.2	1325	2.68	9.3	V, 191+x6		
				1735	31.2	1323	2.68	9.4			
				1718	55.8	1102	2.68	-2.7	V, 191+x2, 162, 159		
				1716	55.8	1101	2.68	-2.6	155, 137		
				1742	49.9	1162	2.68	-1.4	V, 191+, 178, 161		
				1745	49.9	1164	2.68	-1.5	137, 128, 112		
				1683	54.4	1090	2.68	0.0	V, 191+x2, 178	T17	
				1682	54.4	1089	2.68	0.1	137, 125, 109		
				1861	30.9	1422	2.68	3.0	V, 192+x2, 162, 145		
				1860	30.9	1421	2.68	3.1	142, 135		

Pb Bulk Density (kg/m<sup>3</sup>)

M.C. Moisture Content (%)

Pd Dry Density (kg/m<sup>3</sup>)

A.V. Air Voids (%)

S

Shear Strength (P - blows per 50mm on scala penetrometer,

V - shear strength by vane (kPa) in terms of BS: 1377:1975)

S.G. Specific Gravity

R.L. Reduced Level (metres)

## INSITU DENSITY TEST RESULTS

SITE: DONAGAL STUDD, CHAPPLE ROAD

JOB No: 147515.2

TEST NO	DATE	R.L.	SOIL DESCRIPTION	Pb	M.C.	Pd	S.G.	A.V.	SHEAR STRENGTH	RETEST No	COMMENTS
T25	12/12/97		Silt, clayey and slightly sandy, light grey and light brown	1807	30.0	1390	2.68	6.4	V, 192+x3, 163, 151		
T26	15/12/97		Silt, slightly clayey, grey brown and light grey	1805	30.0	1388	2.68	6.5	141		
T27			Silt, slightly clayey, grey brown and light grey	1701	41.3	1204	2.68	5.4	V, 191+x3, 137		
T28			Silt, slightly clayey, grey brown and light grey	1700	41.3	1203	2.68	5.4	128, 124		
T29			Silt, slightly clayey, grey brown and light grey, trace sand	1842	29.4	1423	2.68	5.0	V, 191+x6		
T30	18/12/97		Silt, slightly clayey, grey brown and light grey, trace sand	1843	29.4	1424	2.68	5.0			
T31			Silt, slightly clayey, grey brown and light grey, trace sand	1781	36.5	1305	2.68	3.7	V, 191+x2, 182		
T32			Silt, slightly clayey, grey brown and light grey, trace sand	1782	36.5	1306	2.68	3.6	168, 148, 137		
T33			Silt, slightly clayey, grey brown and light grey, trace sand	1946	24.1	1568	2.68	3.7	V, 191+x6		
T34			Silt, slightly clayey, grey brown and light grey, trace sand	1917	24.1	1544	2.68	5.1			
T35			Silt, slightly clayey, grey brown and light grey, trace sand	1719	47.4	1166	2.68	1.2	V, 192+, 178, 169		
T36			Silt, slightly clayey, grey brown and light grey, trace sand	1720	47.4	1167	2.68	1.1	162, 151, 134		
T37			Silt, slightly clayey, grey brown and light grey, trace sand	1773	43.4	1236	2.68	0.2	V, 192+x2, 169, 149		
T38			Silt, slightly clayey, grey brown and light grey, trace sand	1772	43.4	1236	2.68	0.2	145, 121		
T39			Silt, slightly clayey, grey brown and light grey, trace sand	1922	22.0	1576	2.68	6.6	V, 192+x6		
T40			Silt, slightly clayey, grey brown and light grey, trace sand	1923	22.0	1577	2.68	6.5			
T41			Silt, slightly clayey, grey brown and light grey, trace sand	1639	57.4	1041	2.68	1.4	V, 192+x3, 178, 161		
T42			Silt, slightly clayey, grey brown and light grey, trace sand	1642	57.4	1043	2.68	1.2	157		
T43			Silt, slightly clayey, grey brown and light grey, trace sand	1919	20.7	1590	2.68	7.8	V, 191+, 164, 148	T41	Mixed to blend and dry before recompacting
T44			Silt, slightly clayey, grey brown and light grey, trace sand	1920	20.7	1591	2.68	7.7	111, 88, 84		
T45			Silt, slightly clayey, grey brown and light grey, trace sand	1965	27.0	1547	2.68	0.5	V, UTPx3, 191+x2		
T46			Silt, slightly clayey, grey brown and light grey, trace sand	1964	27.0	1546	2.68	0.5	148		
T47			Silt, slightly clayey, grey brown and light grey, trace sand	1617	46.8	1102	2.68	7.4	V, 182, 164, 162		
T48			Silt, slightly clayey, grey brown and light grey, trace sand	1620	46.8	1104	2.68	7.2	155, 144, 137		

Pb Bulk Density (kg/m<sup>3</sup>)  
M.C. Moisture Content (%)  
Pd Dry Density (kg/m<sup>3</sup>)  
A.V. Air Voids (%)

S Shear Strength (P - blows per 50mm on scala penetrometer,  
V - shear strength by vane (kPa) in terms of BS: 1377:1975)  
S.G. Specific Gravity  
R.L. Reduced Level (metres)

## INSITU DENSITY TEST RESULTS

SITE: DONAGAL STUD, CHAPPLE ROAD

JOB No: 147515.2

TEST NO	DATE	R.L.	SOIL DESCRIPTION	Pb	M.C.	Pd	S.G.	A.V.	SHEAR STRENGTH	RETEST No	COMMENTS
T37	23/12/97		Silt, slightly clayey, light brown, light grey, some grey brown	1769	34.8	1313	2.68	5.4	V,191+x2,164,159,148		
T38	30/12/97		Silt, clayey, light grey	1770	34.8	1313	2.68	5.3			
T39			Silt, clayey, light grey	1720	45.9	1179	2.68	1.9	V,191+x6		
T40			Silt, clayey, light grey	1721	45.9	1179	2.68	1.8			
T41			Silt, slightly clayey, light grey	1786	37.8	1296	2.68	2.6	V,191+x6		
T42			Silt, slightly clayey, light grey	1785	37.8	1295	2.68	2.7			
T43			Silt, slightly clayey, light grey	1940	19.6	1622	2.68	7.7	V,191+x4,164		
T44			Silt, slightly clayey, light grey	1941	19.6	1623	2.68	7.7	148		
T45			Silt, slightly clayey, light grey	1976	20.6	1639	2.68	5.1	V,191+x4,156	T34	
T46			Silt, slightly clayey, light grey	1978	20.6	1640	2.68	5.0	146		
T47			Silt, slightly clayey, light grey	1957	19.6	1637	2.68	6.9	V,191+x6		
T48			Silt, clayey, light grey	1960	19.6	1639	2.68	6.8			
T49			Silt, slightly clayey, light brown and light grey	1762	40.0	1258	2.68	2.7	V,191+x6		Mixed with wet soil before recompacting
T50			Silt, slightly clayey, light brown and light grey	1760	40.0	1257	2.68	2.8			
T51			Silt, slightly clayey, grey and light brown	1952	11.2	1756	2.68	14.9	V,UTPx2,192+x2	T45	
T52			Silt, slightly clayey, grey and light brown	1951	11.2	1755	2.68	14.9	171		
T53			Silt, slightly clayey, grey and light brown	1796	34.7	1333	2.68	4.0	V,UTPx4, 156,143	T44	
T54			Silt, slightly clayey, grey and light brown	1797	34.7	1334	2.68	3.9			
T55			Silt, slightly clayey, light brown, dry	1874	17.9	1590	2.68	12.3	V,UTPx2,174+x2	T48	Excavated to 0.5m and water added before recompacting
T56			Silt, slightly clayey, light brown, dry	1875	17.9	1591	2.68	12.2	169,158		Excavated to 0.5m and water added before recompacting
T57			Silt, slightly clayey, light brown, dry	1670	25.5	1331	2.68	16.4	V,UTPx6	T49	
T58			Silt, slightly clayey, light brown, dry	1672	25.5	1332	2.68	16.3			
T59			Silt, slightly clayey, light brown, dry	1976	22.1	1618	2.68	3.8	V,UTPx6	T46	
T60			Silt, slightly clayey, light brown, dry	1977	22.1	1619	2.68	3.8			

Pb Bulk Density (kg/m<sup>3</sup>)  
M.C. Moisture Content (%)  
Pd Dry Density (kg/m<sup>3</sup>)  
A.V. Air Voids (%)

S Shear Strength (P - blows per 50mm on scala penetrometer,  
V - shear strength by vane (kPa) in terms of BS: 1377:1975)  
S.G. Specific Gravity  
R.L. Reduced Level (metres)

INSITU DENSITY TEST RESULTS

SITE: DONAGAL STUD, CHAPPLE ROAD

JOB No: 147515.2

TEST NO	DATE	R.L.	SOIL DESCRIPTION	P <sub>b</sub>	M.C.	P <sub>d</sub>	S.G.	A.V.	SHEAR STRENGTH	RETEST No	COMMENTS
T49	+15/1/98		Silt, slightly clayey, light grey and light brown	1740 1742	40.8 40.8	1236 1237	2.68 2.68	3.5 3.4	V, 158, 155x2, 145 134, 132	T47	
T50			Silt, slightly clayey, light grey and light brown	1819 1820	40.7 40.7	1293 1293	2.68 2.68	-0.9 -0.9	V, 192+x5, 125		
T51	+19/1/98		Silt, slightly clayey, light brown	1799 1812	25.8 25.8	1430 1441	2.68 2.68	9.8 9.1	V, 174+x2, 169, 158 156, 121		

P<sub>b</sub> Bulk Density (kg/m<sup>3</sup>)  
M.C. Moisture Content (%)  
P<sub>d</sub> Dry Density (kg/m<sup>3</sup>)  
A.V. Air Voids (%)

S Shear Strength (P - blows per 50mm on scala penetrometer,  
V - shear strength by vane (kPa) in terms of BS: 1377:1975)  
S.G. Specific Gravity  
R.L. Reduced Level (metres)

**APPENDIX 3**  
**FILL SPECIFICATION**

## **9.0 EARTHWORKS AND EARTHWORKS CONTROL CRITERIA**

### **9.1 General**

At the time of writing of this report, no earthworks proposals had been provided. Based on the landform, it is assumed that only limited earthworks will take place. These would probably be limited to in-filling of the gullies, with possible some "cut" to provide the materials for the infilling and to equalise the levels across the site. Prior to any placement of engineered fill, any soft, organic or otherwise unsuitable materials should be removed from below the areas to be filled and suitable drainage measures emplaced. These should be sufficient to prevent groundwater from rising through the fill and causing a reduction in the in-situ shear strength of the fill. It may be necessary to culvert the stream, depending on the scheme design. Fill should be placed in layers no more than 0.15m thick when compacted. All fill placed against sloping ground should be properly benched into the natural materials, in benches no greater than 0.5m in height.

If 'cuts' are to be made on the site, it is possible that final ground levels may be close to the level of the organic silts noted in the exploratory holes. If this is the case this could lead to excessive settlement of any buildings constructed in these areas. Consequently it would be necessary to excavate out at least 1m of such voids beneath normal light residential buildings, and fill the void created with an engineered fill. If development other than normal light residential buildings are contemplated, it is recommended, that finalised plans are supplied to Harrison Grierson for further analysis.

### **9.2 Fill Materials and Compaction Criteria**

As the amount of "cut" material produced from earthworks will probably be limited, only one laboratory compaction testing was undertaken. It may be necessary to import suitable material for use as engineering fill.

If the materials arising from the "cut" and any imported materials are cohesive the following criteria are suggested as a guide for earthworks control:

**1. Air Voids Percentage: (As defined in NZS 4402:1986)**

An average value of not more than 10% and no test result permitted to be greater than 12%, in any concurrent group of three tests;

**2. Undrained Shear Strengths:**

An average value of not less than 140kPa and no single result less than 110 kPa, in any group of three tests at any one location;

**3. Moisture Content:**

Not less than 4% of optimum and not less than 2% above optimum.

**APPENDIX 4**  
**STATEMENT OF PROFESSIONAL OPINION**

To: The City Manager  
Manukau City Council  
**MANUKAU**

**STATEMENT OF PROFESSIONAL OPINION AS TO SUITABILITY  
OF LAND FOR RESIDENTIAL DEVELOPMENT**

SUBDIVISION: Donegal Park Stages 1A, 1B & 1C

OWNER/DEVELOPER: Green & McCahill Residential Ltd

LOCATION: Thomas Road

I, Philip Walter Matthew WILLIAMS of HARRISON GRIERSON CONSULTANTS LIMITED,  
429 Parnell Road, Parnell

hereby confirm that:

- 1 I am a Registered Engineer experienced in the field of soils engineering and was retained by the owner/developer as the Soils Engineer on the above subdivision.
- 2 The extent of my inspections during construction and the results of all tests carried out are described in the accompanying report no. 14.7515.1 dated March 1998. The purpose of the report is to provide a record of the earthworks procedures and to describe the technical background upon which this statement of professional opinion has been based. The lots covered by this statement are nos. 1 to 45, 127 to 135, and 193 to 224.
- 3 One purpose of this statement is to describe the extent to which buildings designed in accordance with NZS 3604:1990 "Code of Practice for Light Timber Framed Buildings Not Requiring Specific Design" (NZS 3604) can rely upon soil conditions for foundation construction in accordance with that Code. In this regard the reference to NZS 3604 is itself specific, and does not include other non-specific design codes such as NZS 4229.
- 4 In my professional opinion, not to be construed as a guarantee, I consider that the fill shown on the attached Harrison Grierson Consultant's drawing no. 7515-G01 has been placed in accordance with NZS 4431:1989, Code of Practice for Earthfills for Residential Development and NZS 4404:1981, Code of Practice for Urban Land Subdivision.
- 5 With respect to the safe bearing capacity of soils, in my professional opinion, not to be construed as a guarantee, I consider that:
  - i) The filled ground is suitable for buildings constructed in accordance with NZS 3604 and for which it is believed that the modified soils thereon will afford a foundation safe bearing capacity of 100kPa for shallow foundations.
  - ii) The natural ground and excavated ground comprising all lots except for those referred to in item 5 iii) below, is suitable for buildings constructed in accordance with NZS 3604 and for which it is believed that the unmodified soils thereon will afford a foundation safe bearing capacity of 100kPa for shallow foundations.



- iii) The suitability of natural and excavated ground comprising all or part of the lots 197,198,199,201,202,203, 213, 214, 215 and 216 (all within stage 1B of the subdivision) will be reported on at a later date. These lots are excluded from this certification.

6 Due to the expansive nature of Auckland soils, and of the soils on this site in particular, the following precautions should be observed on all sites:

- i) Conventional shallow pad and strip footings for all buildings be founded at a minimum depth of 450mm below prepared platform levels.
- ii) Where buildings straddle both filled ground and natural or excavated ground, and depending on the nature of the building, allowance be made for possible differential seasonal swelling and shrinking of the disparate soil types.

7 This statement does not extend to retaining walls (including basement excavation retaining walls), or site development cuts or fills which fall within the scope of the Building Act or which require Council resource consent.

8 This statement of professional opinion does not remove the necessity for the usual inspection of foundation excavations by Council and any unexpected or unusual site conditions encountered should in the first instance be referred to Harrison Grierson Consultants Ltd for evaluation.

9 This statement of professional opinion is furnished to the Council and the owner/developer for their purpose alone on the express condition that it will not be relied upon by any other person.

Signed .....

*Way William*

Date .....

*08.04.98*

**DRAWING**

**7515-G01**



I CERTIFY THAT WE HAVE INSPECTED THE FINAL FORMATION OF THIS SUBDIVISION AND, HAVING REVIEWED THIS PLAN IN CONJUNCTION WITH THE KNOWLEDGE OF THE EARTHWORKS CARRIED OUT, ARE SATISFIED THAT THIS IS A TRUE AND ACCURATE RECORD OF THE EARTHWORKS

CERTIFIED allie  
REGISTERED ENGINEERING ASSOCIATE

I CERTIFY THAT, TO THE BEST OF MY KNOWLEDGE, THE FILL CONTOURS SHOWN ON THIS DRAWING ARE ACCURATELY PLOTTED IN RELATION TO LOT BOUNDARIES, AND THAT FILL DEPTHS SHOWN ARE CORRECT

CERTIFIED allie  
REGISTERED ENGINEERING ASSOCIATE  
NB - HEIGHT DATUM, MSL DQSL 1944

- LEGEND
- T 43 DENSITY TEST LOCATION
  - S 1 SCALA PENETROMETER TEST LOCATION

Harrison Graham Consultants Ltd  
P.O. Box 5760  
Wellington St. Auckland

HGCL DRAWING No. 7515-G01

A3:1:1500

WOOD & PARTNERS  
CONSULTANTS LTD.

REGISTERED SURVEYORS  
CONSULTING ENGINEERS.  
72 GRAFTON ROAD BOX 6752 AUCKLAND  
PH 376325, FAX 376336

SCALE: 1:750

SHEET No 1  
OF 1 SHEETS.

CLIENT REF: AC/DANIDOP  
3274

**DONEGAL PARK STG 1A, 1B & 1C**  
DEPTH OF FILL PLAN  
GREEN & MACCAHILL RESIDENTIAL LTD

REVISIONS	DATE	NAME
TEST LOCATIONS ADDED BY HGCL	25/3/96	JF.

DATE MADE: FEB 1999